Wells Street

DIETZGEN

TRADE MARK

ENGINEERS'

LEVEL BOOK

No. 410

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

BOOK 10

Wells St. 2°-24
2°-24
4°-48

C.H.28

WELLS STREET SEC. A
Align't. Sections & Topo. 1-34
Culvits & Slopes 35-72
73

? SURVEY VICINITY Alderman Pond
BUCHNER PROPERTY

B.M. #13 on root of 10" Cherry. Clairdon-Burton Road

Elev of B.M. 1204.32

12.64 1216.96

0.12 1216.84

6.30 1223.14

Intersection of Clairdon-Burton Road

200	150	100	50	℄	50	100	150	200
5.6	5.3	4.6	4.1	4.0	4.3	5.1	5.6	7.2

1219.14

30	25	19	℄	16	18	20	25
3.0	3.2	4.2	4.0	4.1	5.0	4.2	3.9

0+00

1219.14

25	11	10	℄	9	25
2.8	3.8	4.1	4.0	4.0	3.7

1+00

1219.14

25	10	8	℄	8	12	25
2.8	4.1	4.2	4.1	4.2	3.5	4.0

2+00

1219.04

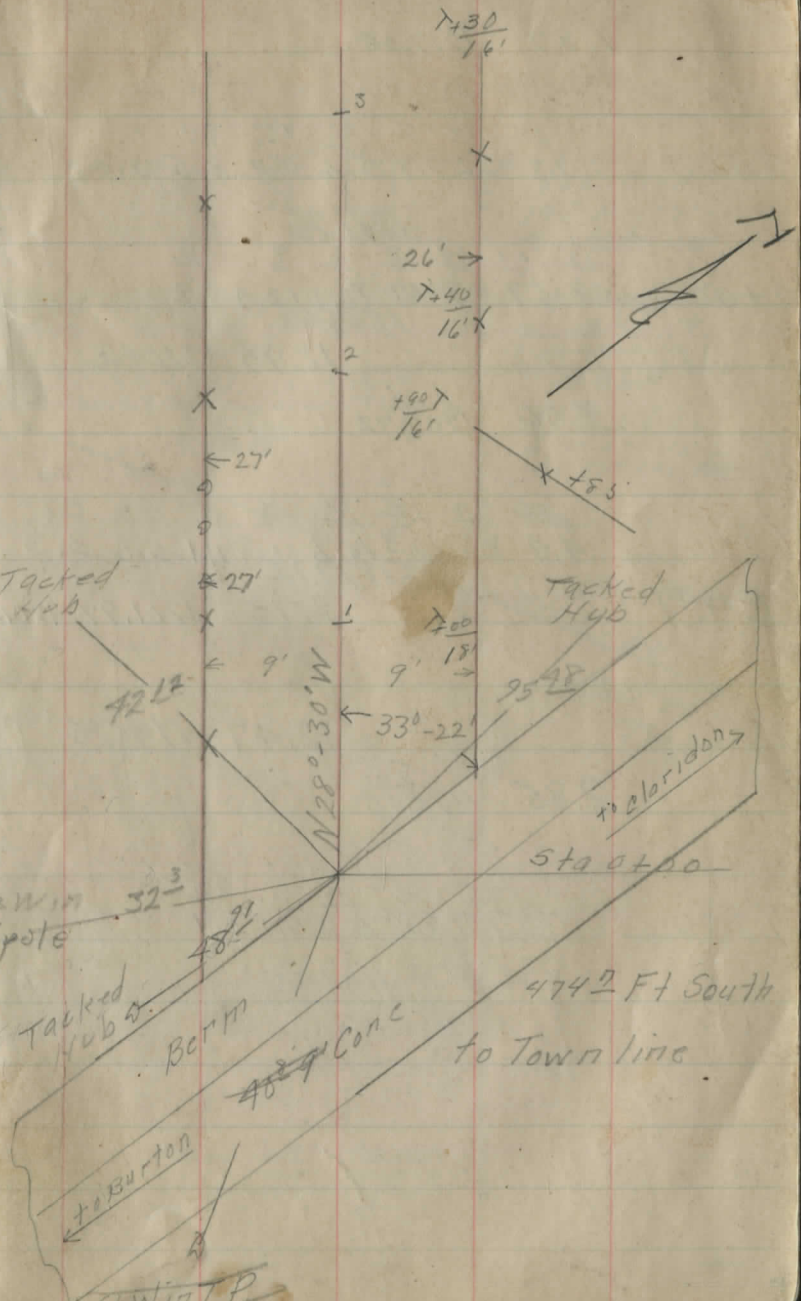
25	12	6	℄	12	14	25
3.2	3.7	6.1	6.2	6.1	5.1	4.5

3+00

1216.94

7.45 1215.69

Note: See book #162 pg 15 for reference of all ℄ points.



1.87 1217.36

	25	14	7	9	15	20	25
4+00	1.2	2.2	5.7	5.6	5.8	3.5	3.2

1211.96

	20	19	14	8	9	9	18
5+00	5.9	6.9	8.3	11.7	13.1	12.4	9.2

1205.46

12.90 1204.66

3.06 1207.72

	25	19	15	9	4	5	20	26
6+00	4.4	8.3	10.3	10.6	10.7	11.1	5.6	5.3

1197.12

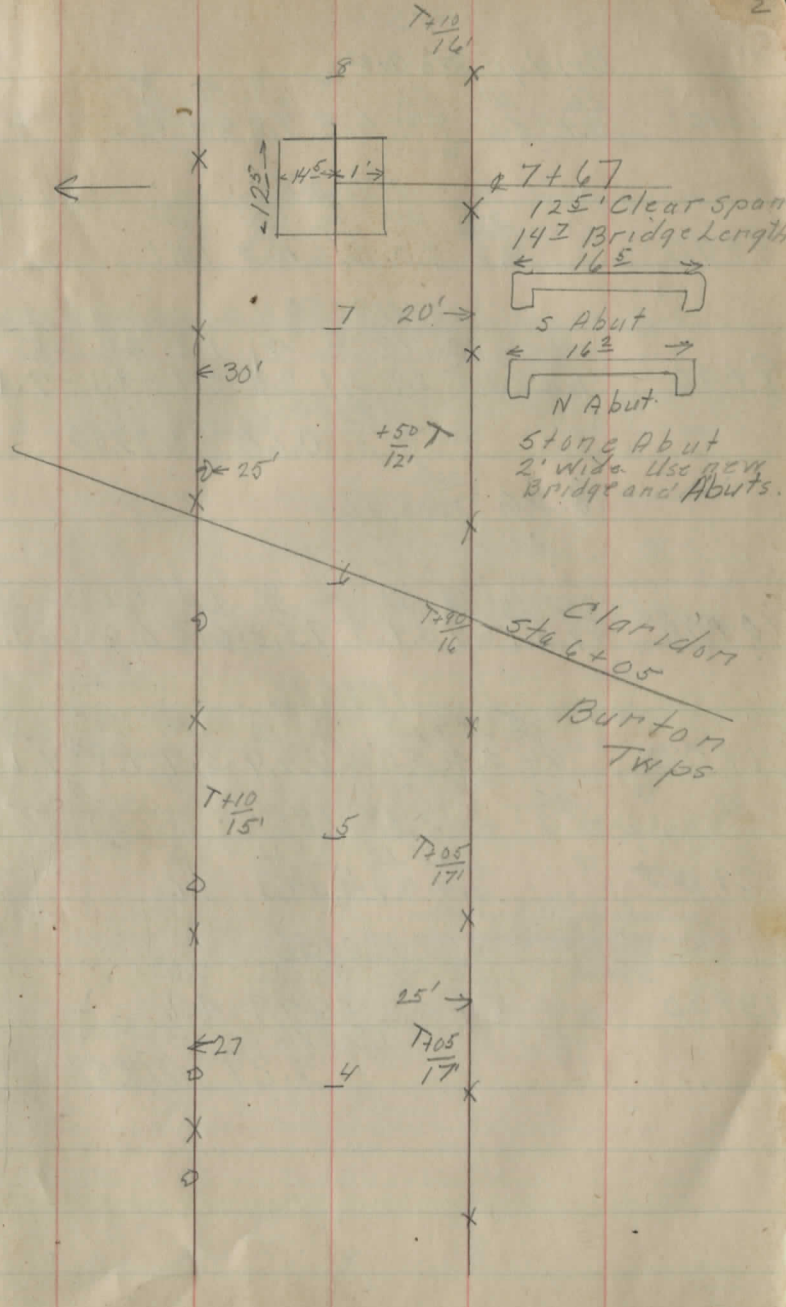
BM#1 5.75 1201.97 1201.75

12.47 1195.25

2.85 1198.10

	25	15	9	3	25
7+00	7.5	6.2	6.2	7.1	8.1

1191.90



1198.10

Bridge Sta. 7+47 ℄

Flows Left	FL	AB	BS		BS	AB	FL
	13.4	6.6	7.7	6.8	7.8	6.4	13.6

1191.30

	25	20	℄	12	25
8+00	8.1	7.0	6.6	10.3	10.1

1191.50

	25	20	19	℄	4	13	20	25
9+00	1.2	3.5	2.7	3.1	2.8	2.7	-4.1	-4.1

1195.00

0.60 1197.50

8.36 1205.86

	25	18	13	11	℄	8	10	12	15	25
10+00	4.9	5.1	6.7	5.4	5.7	5.8	6.3	6.0	5.6	5.6

1206.16

	~~25~~	12	9	℄	6	12	18	25
11+00	4.4	5.4	5.0	4.6	4.9	5.7	4.8	4.6

1201.26

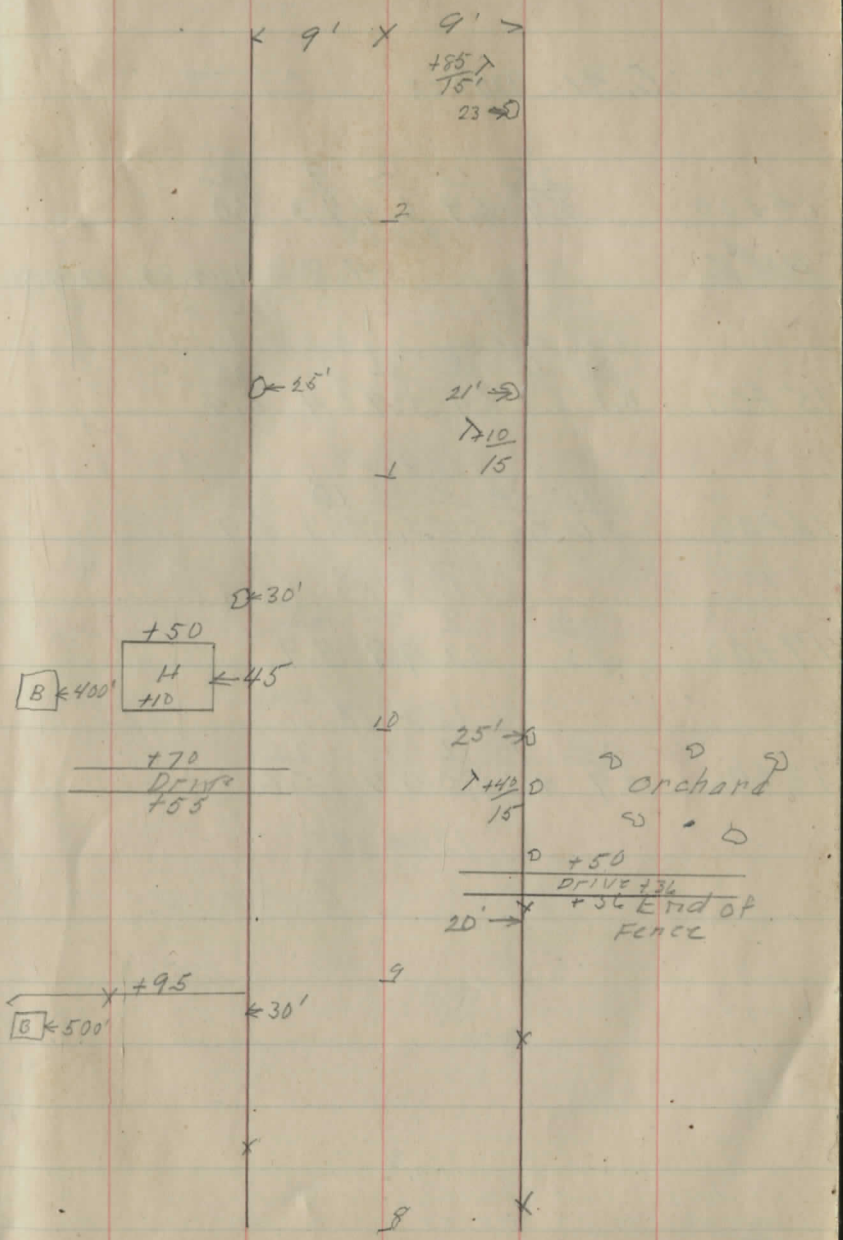
	25	10	℄	11	25
12+00	3.4	4.7	4.3	4.9	3.6

1201.56

	25	10	℄	11	25
13+00	2.4	4.2	3.6	4.4	4.1

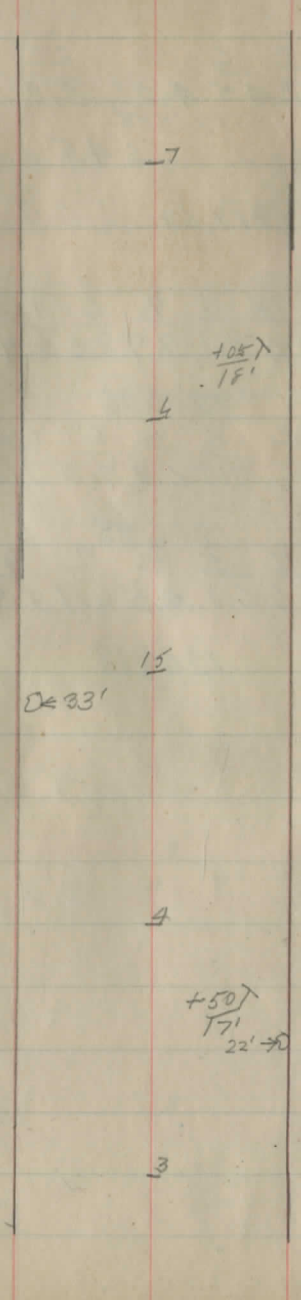
1202.26

3.29 1202.97



6.51 1209.08

	25	15	9	9	25	
14+00	5.9	6.9	6.4	7.3	7.0	
		1202.68				
BM #2			4.23	1204.85		1204.86
	25	18	8	9	8	25
15+00	5.1	6.3	6.4	5.9	6.4	6.4
			1203.18			
	25	14	8	9	10	25
16+00	2.6	5.5	5.5	5.0	5.7	5.7
			1204.08			
	25		9	9	25	
17+00	3.5		5.2	4.9	5.9	
			1204.18			
	25	10	7	9	25	
18+00	4.9	4.6	5.0	4.7	5.6	
			1204.38			



120.08

19+00 — 25 @ 4.7 | 8 @ 4.2 | C @ 4.5 | Q @ 4.0 | 25 @ 5.0

120.68

3.45 120.63

8.05 1213.68

20+00 — 25 @ 6.8 | 14 @ 8.0 | 6 @ 8.1 | Q @ 7.7 | 6 @ 8.0 | 12 @ 8.4 | 25 @ 8.6

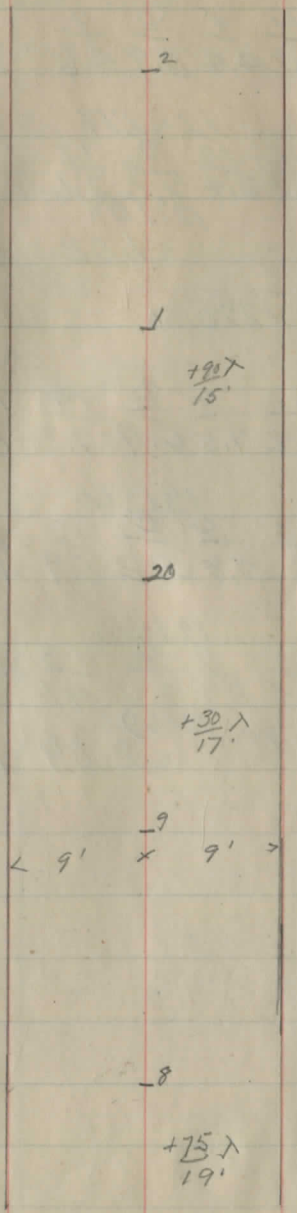
120.98

21+00 — 25 @ 4.6 | 6 @ 7.2 | Q @ 6.8 | 6 @ 7.3 | 12 @ 7.2 | 18 @ 6.4 | 25 @ 6.6

120.88

22+00 — 25 @ 3.8 | 7 @ 5.6 | 5 @ 6.0 | E @ 5.5 | 7 @ 6.1 | 9 @ 5.7 | 25 @ 4.6

120.18



1213.68

23+00	25	10	6	Ø	8	25	
	1.8	4.1	4.4	3.9	4.6	2.3	

1209.78

24+00	25	16	10	Ø	13	15	25
	-1.4	-0.8	2.4	1.6	2.6	1.3	1.0

1212.08

1.02 1212.68

7.64 1220.30

25+00	25	10	8	Ø	14	16	25
	5.1	5.2	7.5	6.7	7.3	6.8	5.7

1213.60

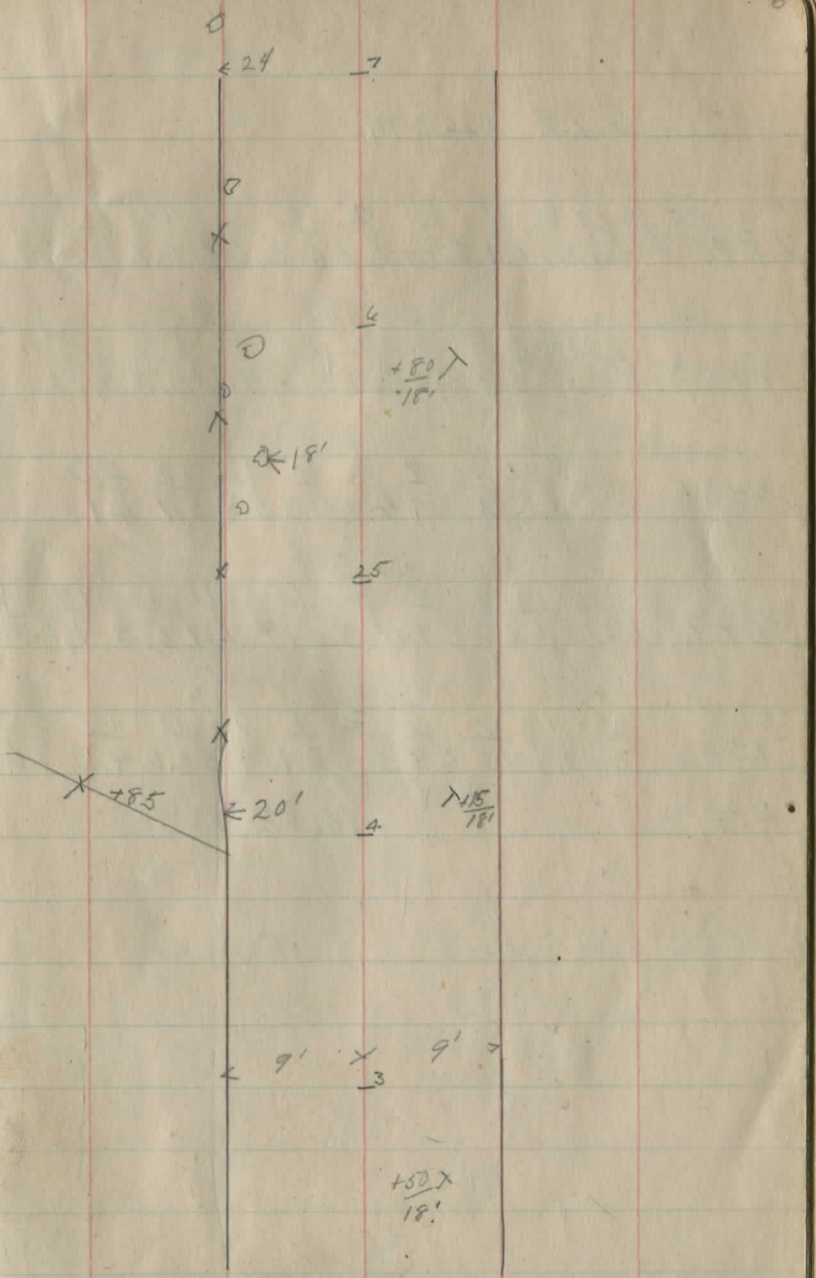
26+00	25	13	9	Ø	13	19	25
	3.2	3.9	5.8	5.2	5.7	4.2	4.2

1215.10

27+00	25	9	Ø	13	18	25
	2.5	3.9	3.4	4.6	3.2	2.7

1216.90

BM #3 2.09 1218.21 1218.20



5.77 1223.97

	25 5.3	16	13	8	7	5	0	10	11	12	25
28+00	5.3	6.4	5.9	6.1	5.7	5.4	6.2	6.6	6.2	4.7	

1218.57

	25	10	8	8	6	10	11	12	25	
28+00	4.8	5.5	5.8	5.4	4.3	5.3	5.6	5.3	4.2	

1219.67

	25	11	10	9	0	11	12	13	25	
30+00	4.5	5.0	5.8	5.4	4.7	5.0	5.8	5.1	4.1	

1219.27

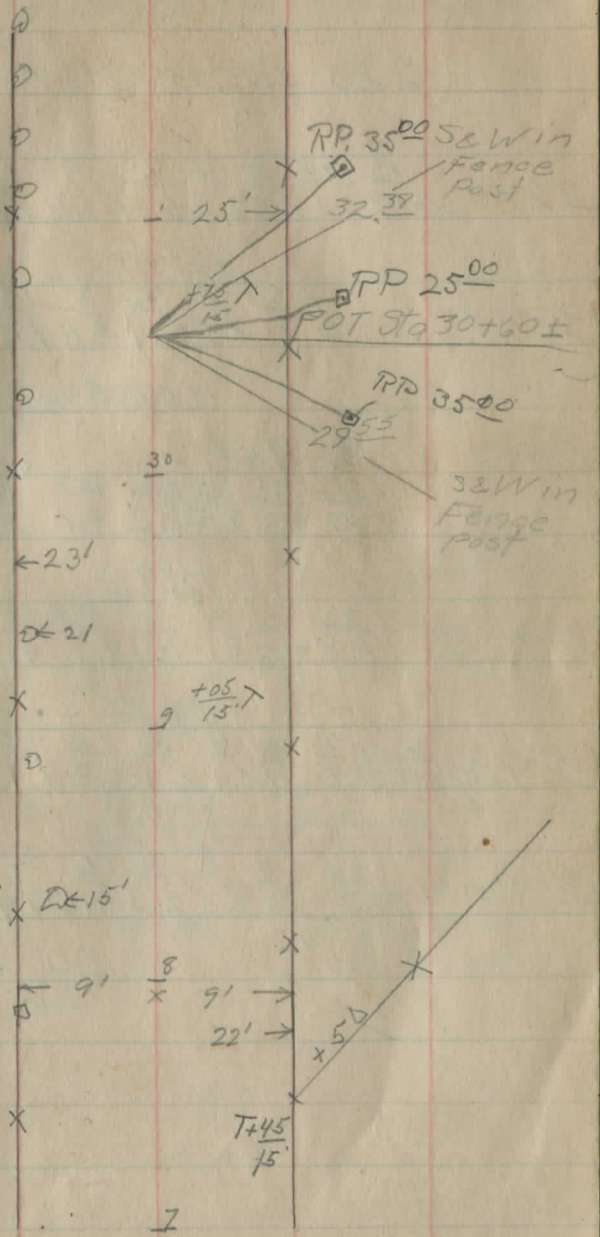
	25	15	11	9	8	6	10	11	12	17	25
30+75	3.6	3.7	5.4	6.2	5.3	4.3	5.4	6.1	5.3	4.1	4.1

1219.67

	25	13	7	5	0	9	10	11	17	25	
31+00	3.8	3.9	7.5	6.4	5.5	6.6	7.3	6.6	4.2	3.6	

1218.47

10.82 1213.15



2.20 1215.35

	25	14	5	4	2	9	10	17	26
32+00	-1.2	0.0	6.3	5.7	5.4	5.7	6.5	3.6	0.9

1209.95

	25	6	2	8	13	25
33+00	9.8	8.5	8.1	8.0	10.1	11.3

1207.25

Bridge

FL	Ab	BS		DS	Ab	FL
13.7	8.3	9.5	8.2	9.6	8.3	12.1

1207.15

	25	5	4	2	8	25
34+00	8.8	7.6	8.1	7.7	7.9	9.4

1207.65

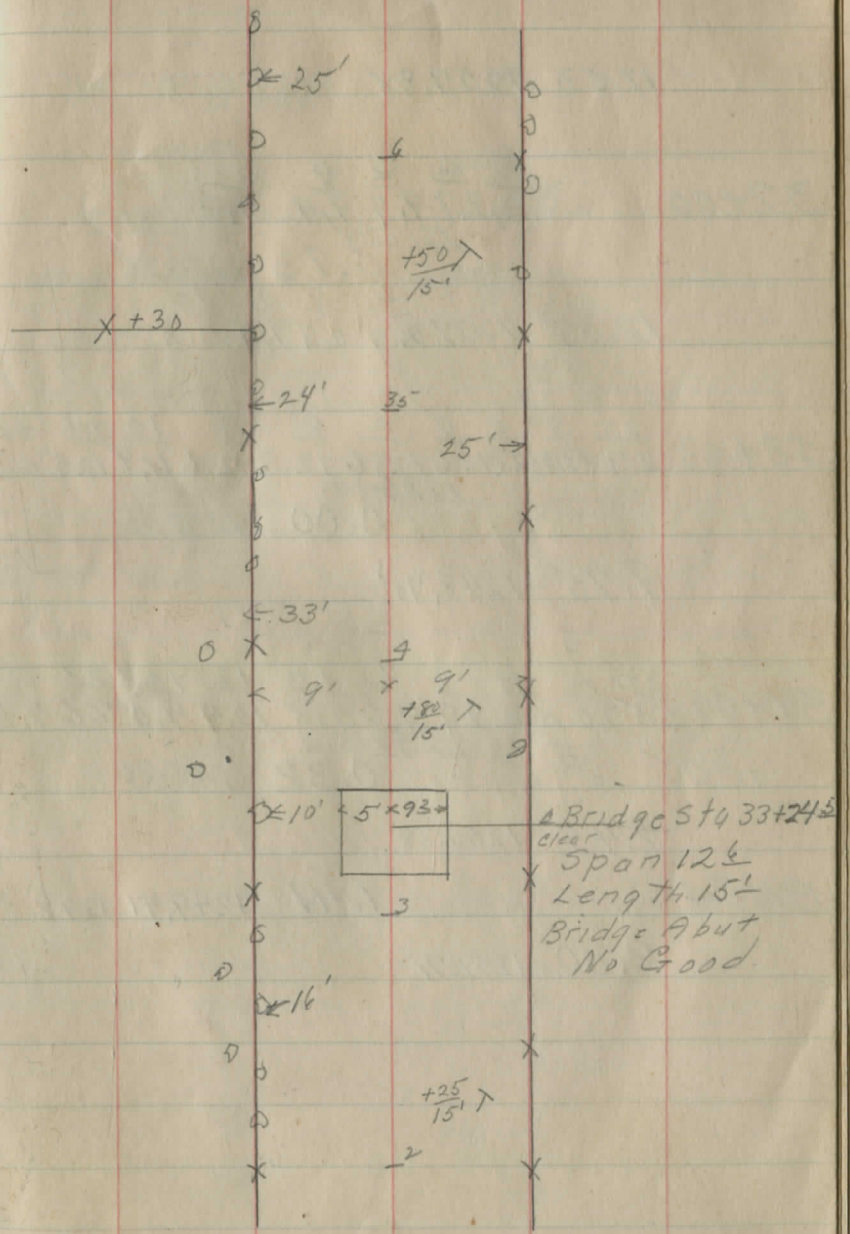
	25	12	8	5	4	2	12	13	14	23
35+00	5.1	6.2	6.8	5.6	6.1	6.1	6.2	6.4	6.1	5.2

1209.25

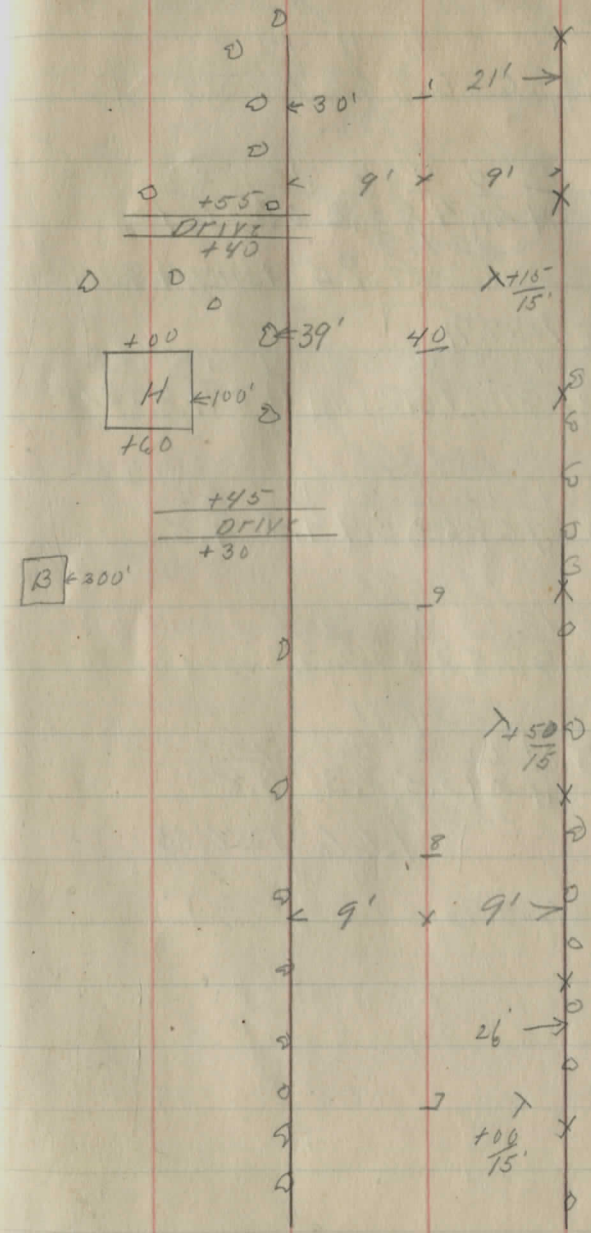
	25	7	5	2	6	8	25
36+00	1.8	3.0	2.2	2.5	2.6	1.9	1.8

1212.85

0.00 1265.35



				12.53			1227.88				
37+00	25	6	4	9	25						
	9.3	9.7	9.9	9.4	9.3						
				1217.88							
						8.93	1226.95				
				12.05			1239.00				
38+00	25	9	8	7	4	8	9	10	14	25	
	2.7	13.0	12.2	12.6	12.6	12.2	12.6	11.9	10.5	6.5	
				1226.40							
						0.00	1239.00				
				9.75			1248.75				
39+00	25	16	10	9	4	10	12	15	21	25	
	5.5	7.0	10.3	9.7	9.6	9.8	10.4	9.0	7.6	7.6	
				1239.15							
						0.32	1248.43				
				2.45			1250.88				
BM #4						1.47	1249.41	1249.39			
				2.30			1251.71				



1251.71

40+00 — 25/4.0, 13/4.8, 8/7.2, 7/6.8, ℄/6.7, 7/6.9, 12/7.0, 25/3.5

1245.01

41+00 — 25/2.8, 12/5.4, 7/4.9, ℄/4.8, 6/5.2, 10/5.5, 25/6.1

1246.91

4.22 1247.49

10.22 1257.71

42+00 — 25/10.8, 13/10.8, 8/10.2, ℄/10.2, 3/10.1, 7/11.2, 13/11.8, 25/12.6

1247.51

43+00 — 25/2.6, 22/3.0, 13/6.4, 12/6.2, ℄/6.0, 5/5.9, 11/4.5, 25/4.5

1251.71

43+50 — 25/0.9, 19/1.3, 13/2.5, ℄/3.0, 25/2.2

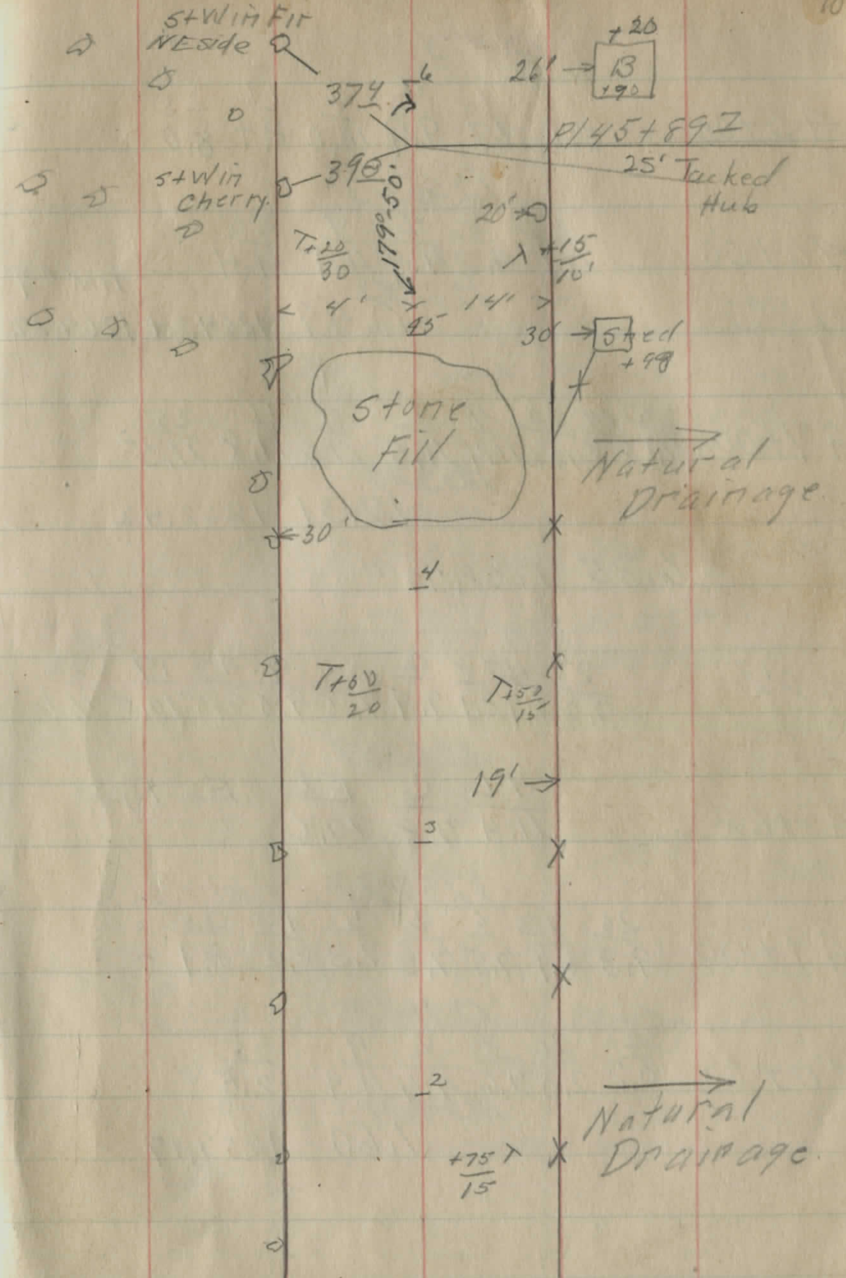
1254.71

44+00 — 25/2.1, 14/1.1, 10/3.9, ℄/3.5, 15/3.3, 25/3.8

1254.21

1.66 1256.05

8.68 1264.73



1264.73

45+00 — 25 / 8.1 — 13 / 9.9 — 9 / 9.7 — 4 / 10.0 — 11 / 8.4 — 25 / 8.0

1255.03

46+00 — 25 / 2.1 — 8 / 4.2 — 9 / 4.9 — 25 / 4.1 — 4.4

BM. #5 — 1252.83 — 0.49 — 1264.24 — 1264.22

B.M. #5

47+00 — 25 / 2.1 — 19 / 8.5 — 10 / 12.0 — 4 / 11.4 — 9 / 11.5 — 11 / 11.6 — 11.8 — 25 / 11.5

1253.23 — 12.31 — 1252.42

6.35' — 1258.77

48+00 — 25 / 7.0 — 15 E / 8.7 — 8.1 — 9 / 7.9 — 5 / 7.8 — 9 / 9.0 — 13 / 9.5 — 19 / 10.3 — 25 / 11.6

1250.87

48+68 — FL / 11.4 — 9 / 7.8 — EL / 10.6 — EL Right

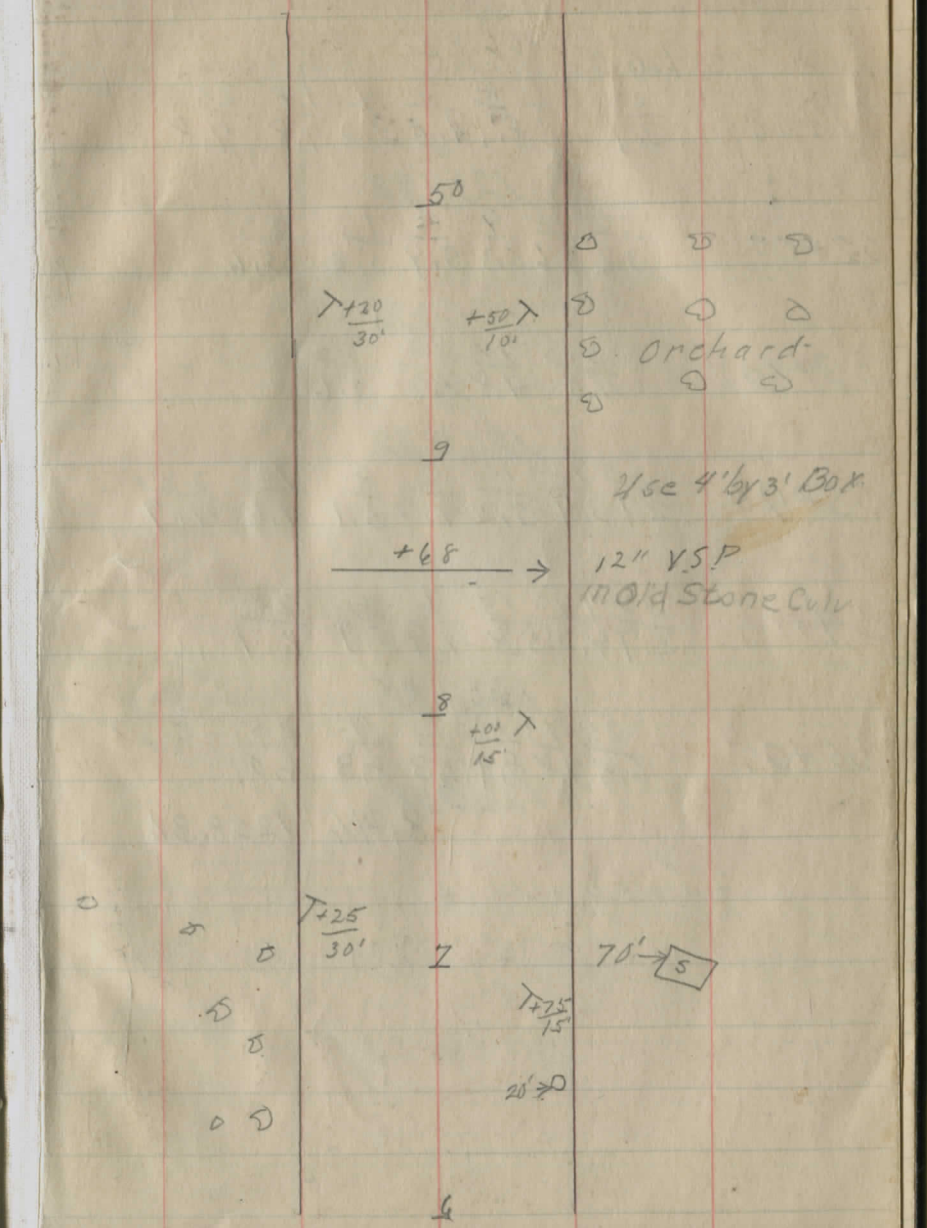
1250.97

49+00 — 25 / 9.3 — 13 / 8.1 — 6 / 7.5 — 9 / 7.3 — 2 / 7.3 — 10 / 8.2 — 25 / 8.1

1251.47

50+00 — 25 / 0.2 — 16 / 2.0 — 8 / 4.6 — 9 / 4.4 — 7 / 4.4 — 25 / 2.6

1254.37 — 1.60 — 1257.17



9.65 1264.82

51+00	25	15	E	E	7	14	25
	3.7	6.1	8.7	9.8	9.0	7.8	7.8

1257.82

52+00	25	16	9	E	10	25
	3.2	3.6	5.3	5.9	5.2	5.6

1260.72

53+00	25	14	E		25
	4.0	4.8	4.5		5.6

1262.32

53+70	25	16	14	E	8	10	25
	2.7	3.9	5.2	4.2	5.1	4.6	4.7

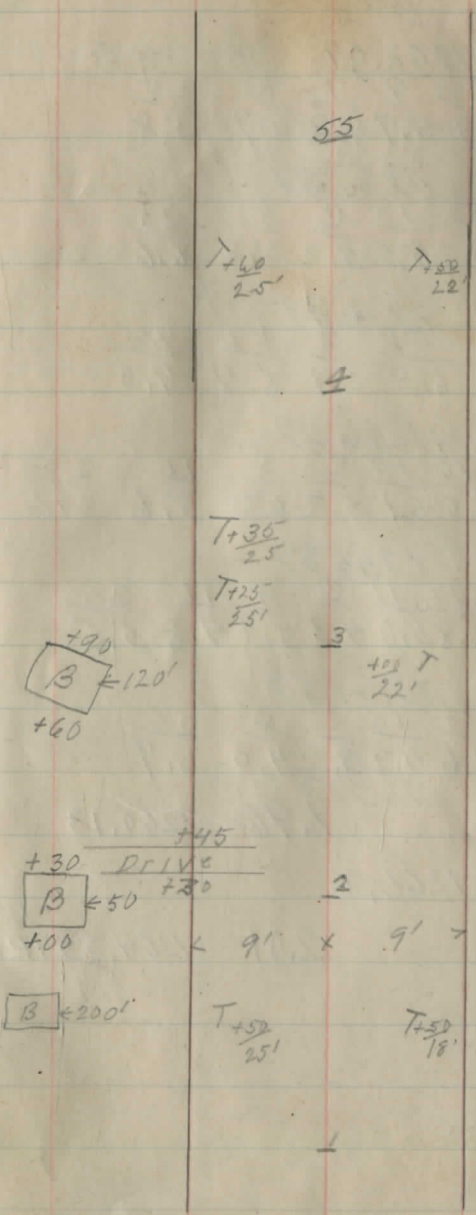
1262.62

54+00	25	12	13	E	8	25
	2.7	4.2	5.8	4.9	5.9	6.1

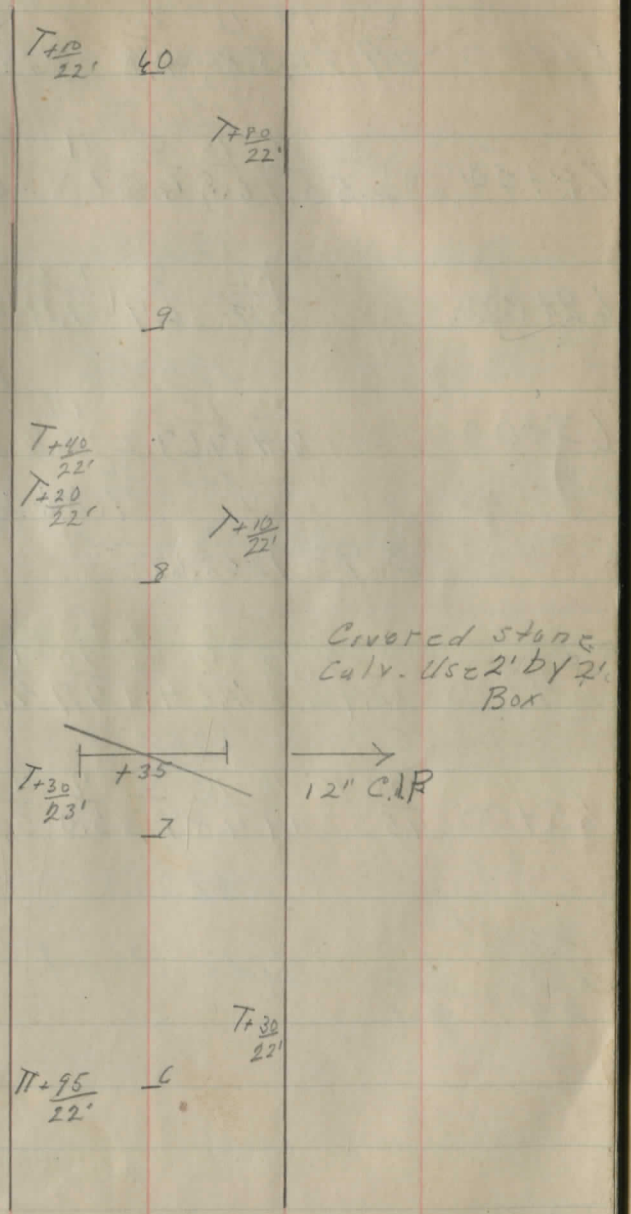
1261.92

55+00	25	13	10	E	9	25
	6.6	7.8	8.4	7.3	8.3	8.0

1259.58 8.46 1258.36



	3.73	1262.09						
	(25)	9	8	8		(25)		
56+00	3.3	4.7	4.2	5.3		5.8		
		1257.89						
	(25)	(13)	8	5		(25)		
57+00	4.3	5.5	5.2	5.2		6.6		
		1256.89						
	FL	8	FL	(30)				
57+35	6.3	5.1	6.4	7.5				
		1256.99						
	(25)	(16)	(14)	8	8	(11)	(25)	
58+00	4.3	5.5	6.1	5.2	6.2	5.6	5.6	
		1256.89						
	(25)	(15)	(12)	(11)	8	9	(11)	(25)
59+00	3.2	3.0	5.8	5.0	4.5	5.1	4.8	5.5
		1257.59						
	(25)	(18)	(12)	8		(23)		
60+00	2.2	2.6	4.2	3.2		4.0	3.9	
		1258.84						
			1.96	1260.13				
	6.43	1266.56						
BM #6			2.01	1264.55	BM #6	1264.53		



126656

61+00	25 / 2.9	17 / 3.2	11 / 5.8	℄ / 4.8	8 / 5.6	17 / 4.9	25 / 4.7

126176

62+00	25 / 4.5	19 / 5.1	10 / 6.9	℄ / 6.0	11 / 6.8	25 / 5.5

126056

	FL	℄	FL
62+83	6.9	6.7	7.9

125986

63+00	25 / 7.4	18 / 7.6	℄ / 7.2	14 / 7.8	25 / 7.9

125136

7.86 125870

3.93 126263

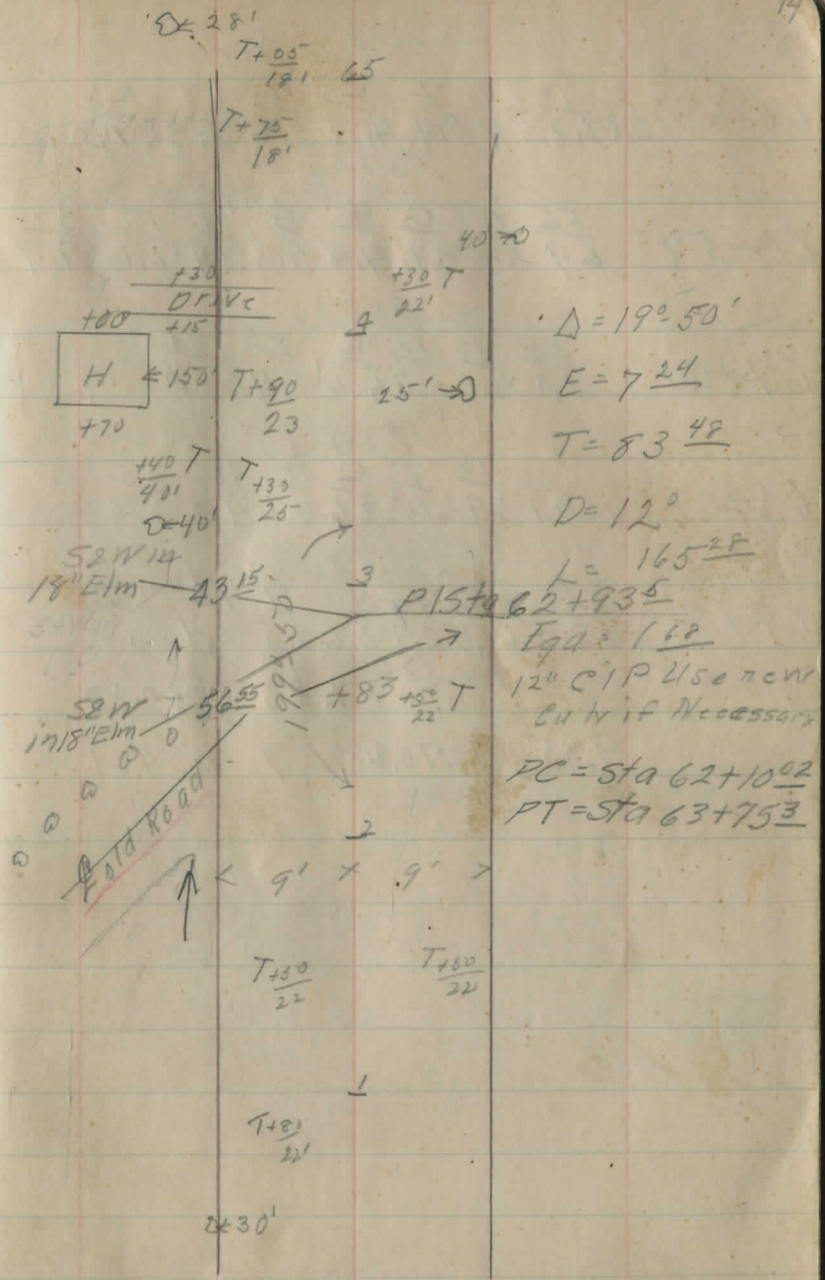
64+00	25 / 2.9	19 / 4.2	9 / 4.6	℄ / 4.1	10 / 4.7	12 / 4.2	25 / 4.6

125853

65+00	25 / 4.5	19 / 5.2	18 / 4.9	10 / 4.8	℄ / 4.3	7 / 5.0	25 / 5.8

125833

150 / 2.4 — 100 / 4.1 — Side Road 7.1



1262.63

66+00	25	16	14	7	℄	7	13	25
	5.8	5.8	5.4	5.4	4.8	5.6	5.3	6.0

1257.83

Bridge

66+54	FL	H	G	℄	℄	H	FL	50
	6.9	3.5	4.4	4.4	4.3	3.4	6.6	7.9

1258.23

67+00	25	12	10	℄	8		25
	5.1	4.6	5.3	4.4	5.4		5.8

1258.23

68+00	25	12	9	℄	8	11	25
	4.1	3.9	4.5	3.6	4.6	4.2	5.0

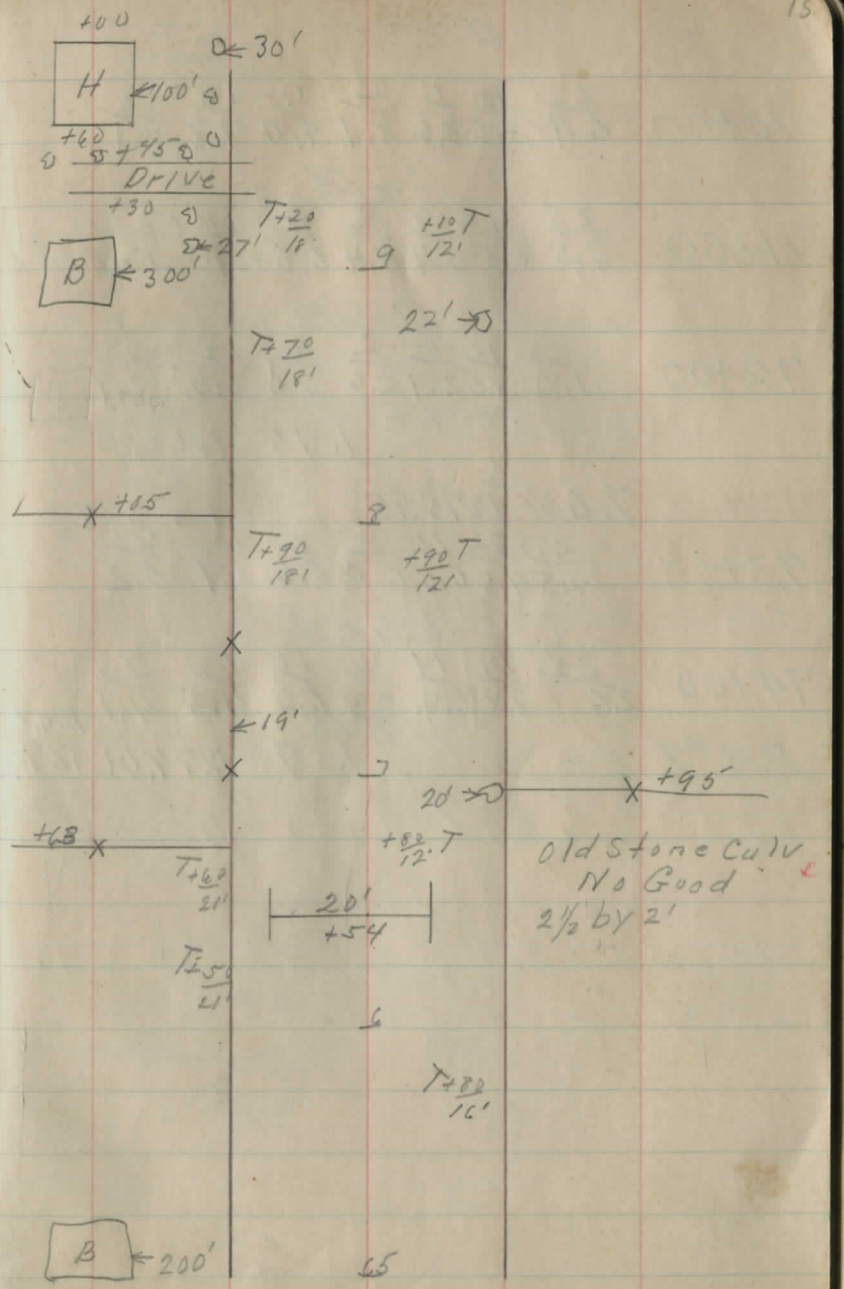
1259.03

69+00	25	20	18	14	℄	7	10	25
	0.9	2.6	1.6	2.4	2.6	3.5	2.4	2.2

1260.03

1.80 1260.83

9.85 1270.68



1270.68

70+00	25 / 6.9	18 / 8.6	11 / 8.6	C / 8.1	17 / 9.0	13 / 7.8	25 / 8.1

1262.58

71+00	25 / 2.5	13 / 6.5	9 / 5.7	C / 5.4	8 / 6.5	14 / 5.0	25 / 5.8

1265.28

72+00	25 / 1.0	11 / 3.5	8 / 2.9	C / 2.6	8 / 3.6	14 / 2.5	25 / 2.7

1268.08
1.75 1268.93

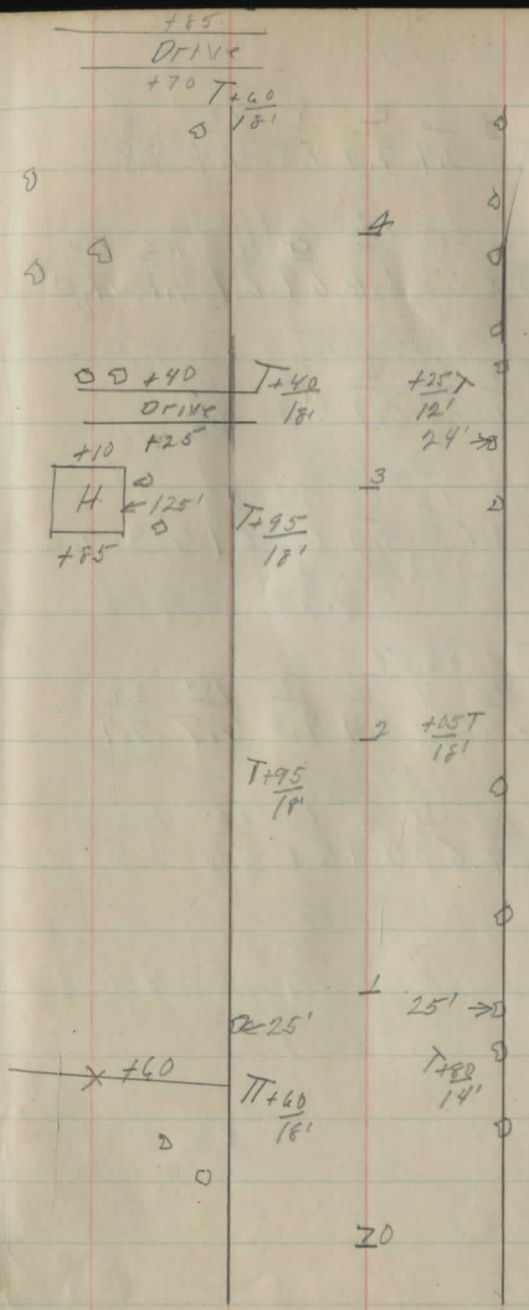
7.05 1275.98

73+00	25 / 4.5	22 / 4.5	11 / 6.5	C / 6.0	8 / 6.6	15 / 5.1	25 / 5.2

1269.98

74+00	25 / 2.6	19 / 3.8	14 / 6.4	C / 5.8	10 / 6.0	13 / 4.3	25 / 4.1

BM #7 1270.68
1.37 1274.61 1274.5



1275.98

75+00 25 16 12 12 8 12 25
5.6 7.0 7.4 7.0 7.8 7.4 8.8

1268.98

Bx 1492

75+63 FL H 6 6 6 H FL 50
9.1 5.8 6.8 6.6 6.9 6.1 9.1 11.0

1269.38

76+00 25 13 12 12 25
7.4 7.3 6.7 7.3 8.5

1269.28

77+00 25 12 13 12 10 12 17 25
2.6 6.3 6.5 5.0 6.3 6.1 4.3 4.2

1270.98

4.54 1271.44

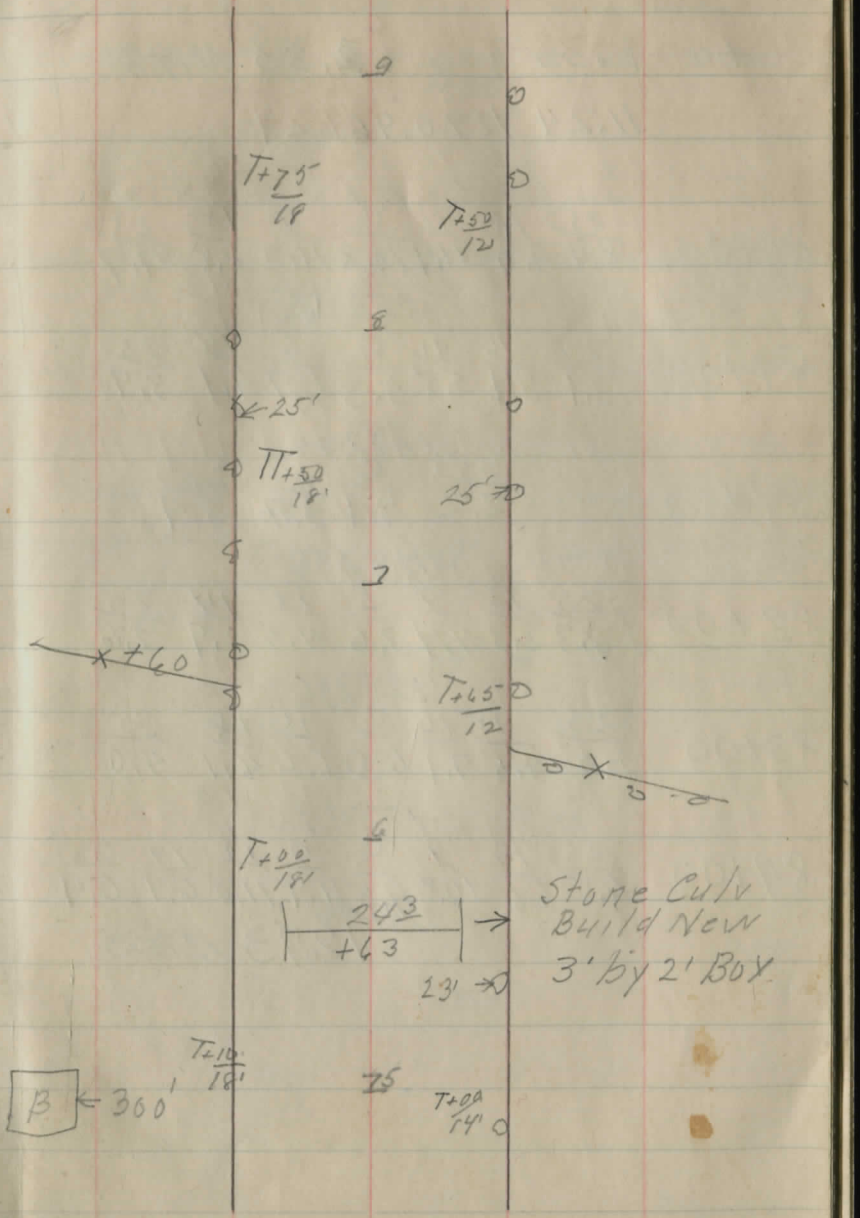
10.63 1282.07

78+00 25 12 9 9 9 14 25
7.0 10.0 8.9 8.4 9.3 7.7 7.9

1273.67

79+00 25 19 11 9 11 16 25
4.4 4.4 6.3 4.9 6.1 3.7 4.5

1277.17

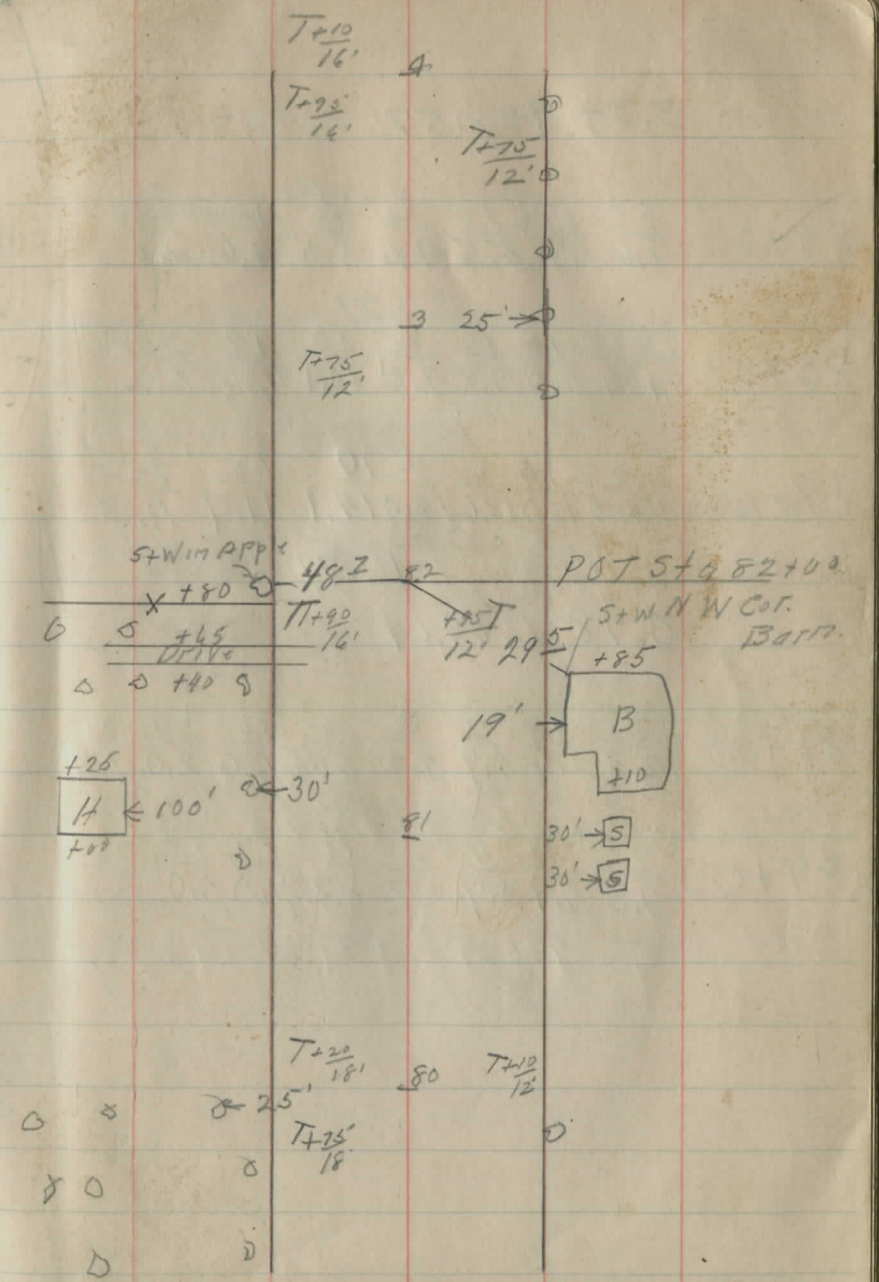


2.35 1279.72

11.24 1290.96

80+00	25	18	11	9	9	18	25
	8.4	9.0	11.4	10.8	11.3	8.8	7.7
	1280.16						
81+00	25	16	11	9	6	14	25
	3.1	3.4	5.5	5.3	5.7	4.1	3.7
	1285.66						
81+50	25	9	14	25			
	2.2	3.1	3.7	3.4			
	1287.86						
82+00	25	16	9	9	10	14	25
	3.3	2.3	4.4	3.6	4.5	2.9	2.6
	1287.36						
83+00	25	18	10	9	11	18	25
	4.6	4.8	7.1	6.0	6.6	4.1	4.0
	1284.96						
84+00	25	19	9	9	2	11	19	25
	6.5	6.6	10.8	9.5	9.9	11.0	6.4	6.4
	1281.46							

12.73 1278.23



3.34 | 281.57

85+00	25	19	10	C	8	15	25	
	1.6	1.7	5.5	4.6	5.5	1.6	1.0	

127.97

86+00	25	19	15	10	C	10	19	25
	7.1	7.1	9.0	9.8	9.2	10.1	6.8	6.2

127.37

87+00	25	14	6	C	10	18	25	
	11.3	12.0	13.6	13.0	14.1	11.7	11.3	

126.57

12.71 | 126.86

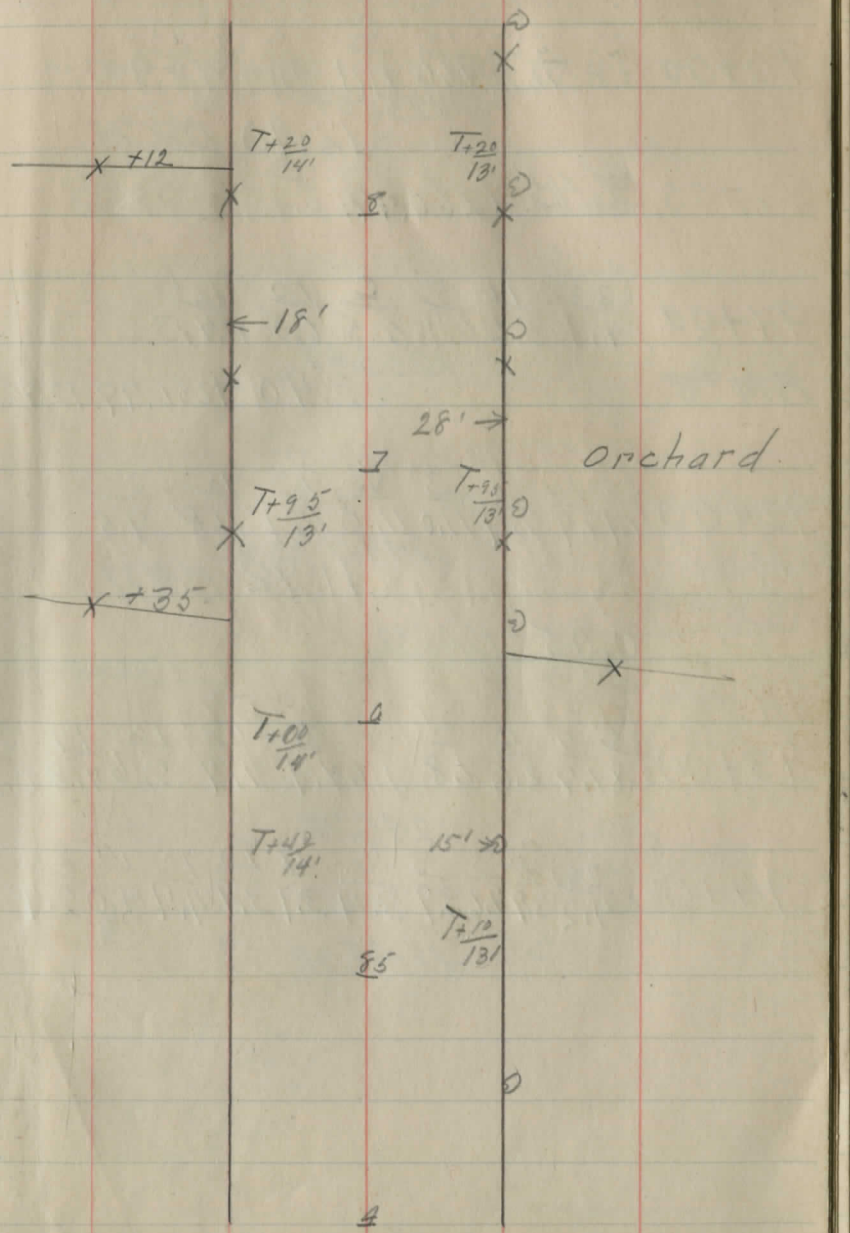
0.78 | 126.64

88+00	25	13	7	C	8	10	20	25
	2.3	2.6	5.9	5.2	5.6	6.6	2.0	1.4

126.44

89+00	25	11	7	C	11	13	23	25
	7.3	7.9	8.7	8.2	8.2	9.0	5.0	5.0

126.44



1269.64

90+00 25/11.2 10/11.6 C/11.1 9/11.2 23/8.9

1258.54 12.90 1256.74

3.45 1260.19

91+00 23/4.1 14/3.6 5/6.9 C/6.5 10/6.5 25/4.3

1253.69

BM #8 3.40 1256.79 1256.74

92+00 20/9.4 14/9.9 5/12.1 3/11.0 C/11.0 13/11.1 15/11.8 25/9.6

1249.19 1.92 1248.27

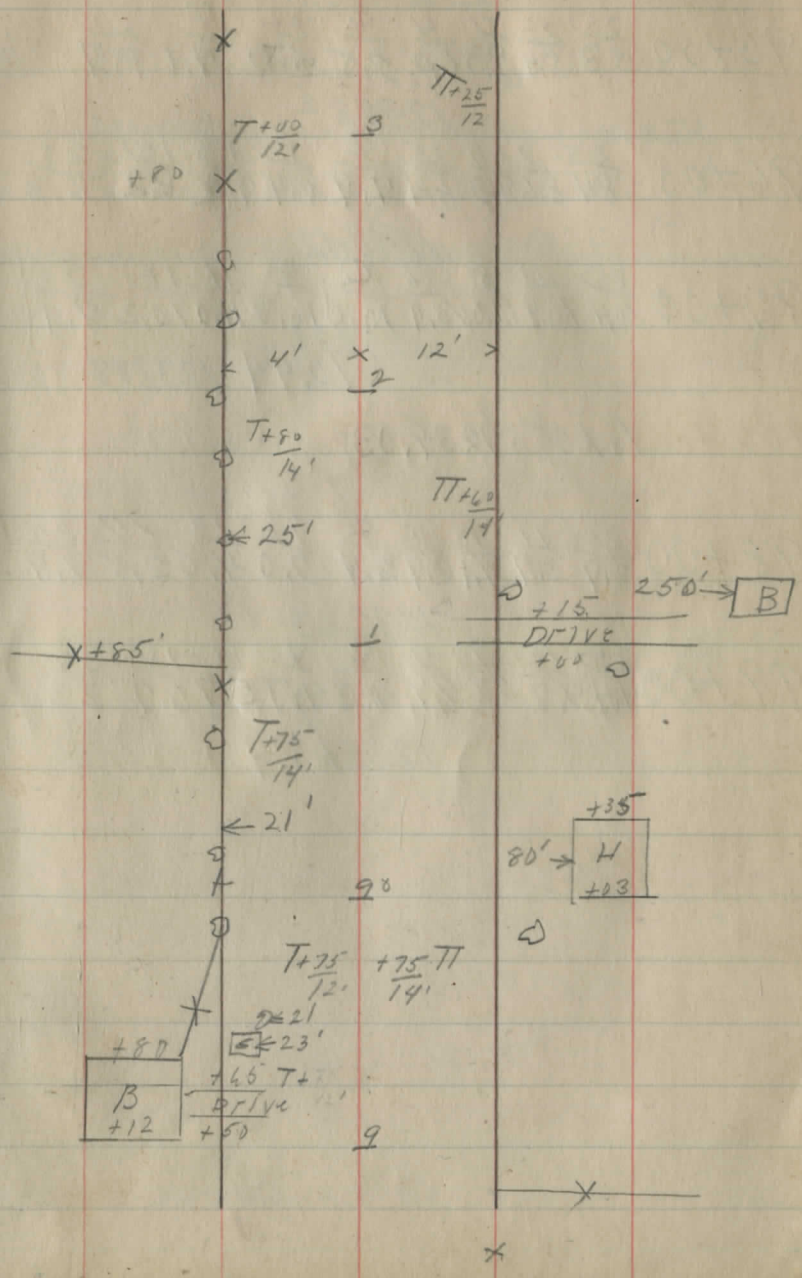
0.05 1248.32

93+00 25/2.8 7/1.7 4/2.6 2/1.8 C/1.6 5/1.1 13/1.9 15/2.6 17/1.8 25/2.5

1246.72

94+00 25/4.2 8/3.9 3/4.6 3/3.9 C/3.4 4/3.1 10/3.9 12/4.7 14/4.0 25/2.4

1244.92



124832

95+00 25 3.3 12 5.4 9 9.2 4 6.0 9 6.0 13 5.5 14 6.0 25 9.1 25 8.7

124282

96+00 25 8.4 9 8.6 9 9.3 5 8.4 9 7.9 11 8.4 13 9.2 15 8.2 25 6.3

124042

97+00 25 10.4 11 10.4 8 11.0 6 10.4 9 10.0 11 6.3 11.0 10.2 25 9.1

123832

10.44 123788

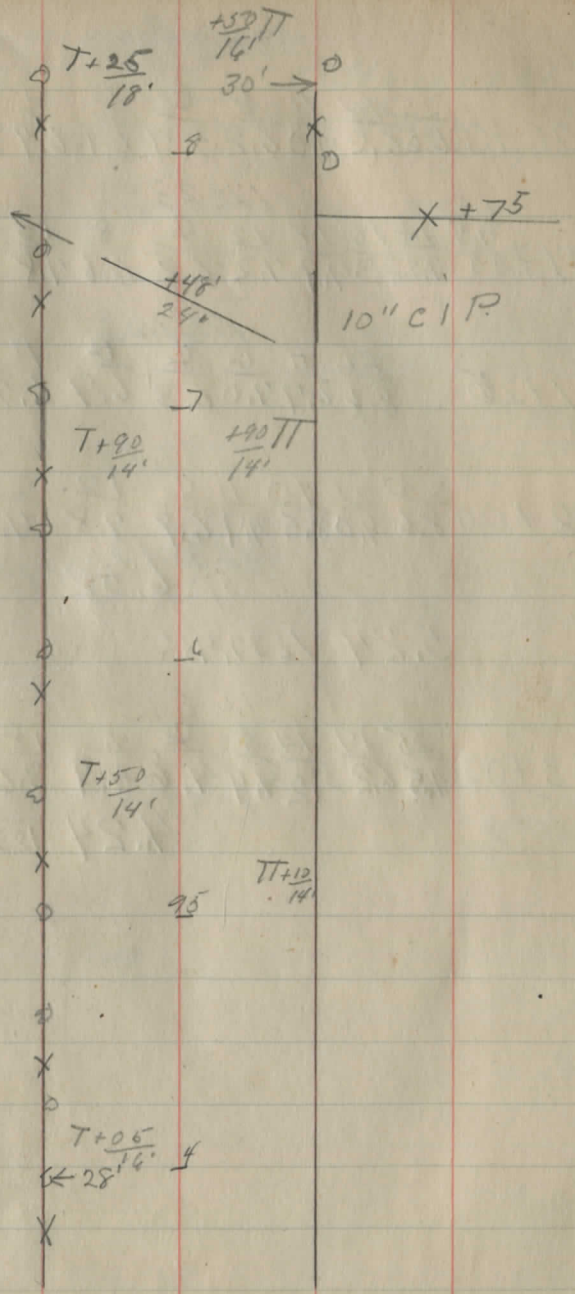
1.15 123903

98+00 25 2.9 11 2.7 10 4.1 6 2.9 9 2.4 14 3.0 13 4.0 17 2.5 25 1.9

123663

99+00 25 4.4 12 4.7 9 3.8 7 4.9 9 4.0 11 4.7 14 5.7 18 3.7 25 3.3

123503



123.03

	25	14	11	8	C	8	11	13	20	20	
100+00	6.6	6.2	7.0	6.2	5.7	6.1	6.9	6.1	4.9	4.9	

123.33

	25										
	7.5	LE	16	14	12	C	8	13	25		
101+00	7.5	8.3	7.9	7.2	6.2	6.6	7.8	6.3			

123.83

	FL	11	C	C	C	#	FL				
101+25	8.6	6.7	7.0	6.3	6.7	6.5	8.3				

123.73

	25	21	10	11	C	12	25				
102+00	8.6	9.0	8.5	7.7	6.8	7.8	7.2				

123.13

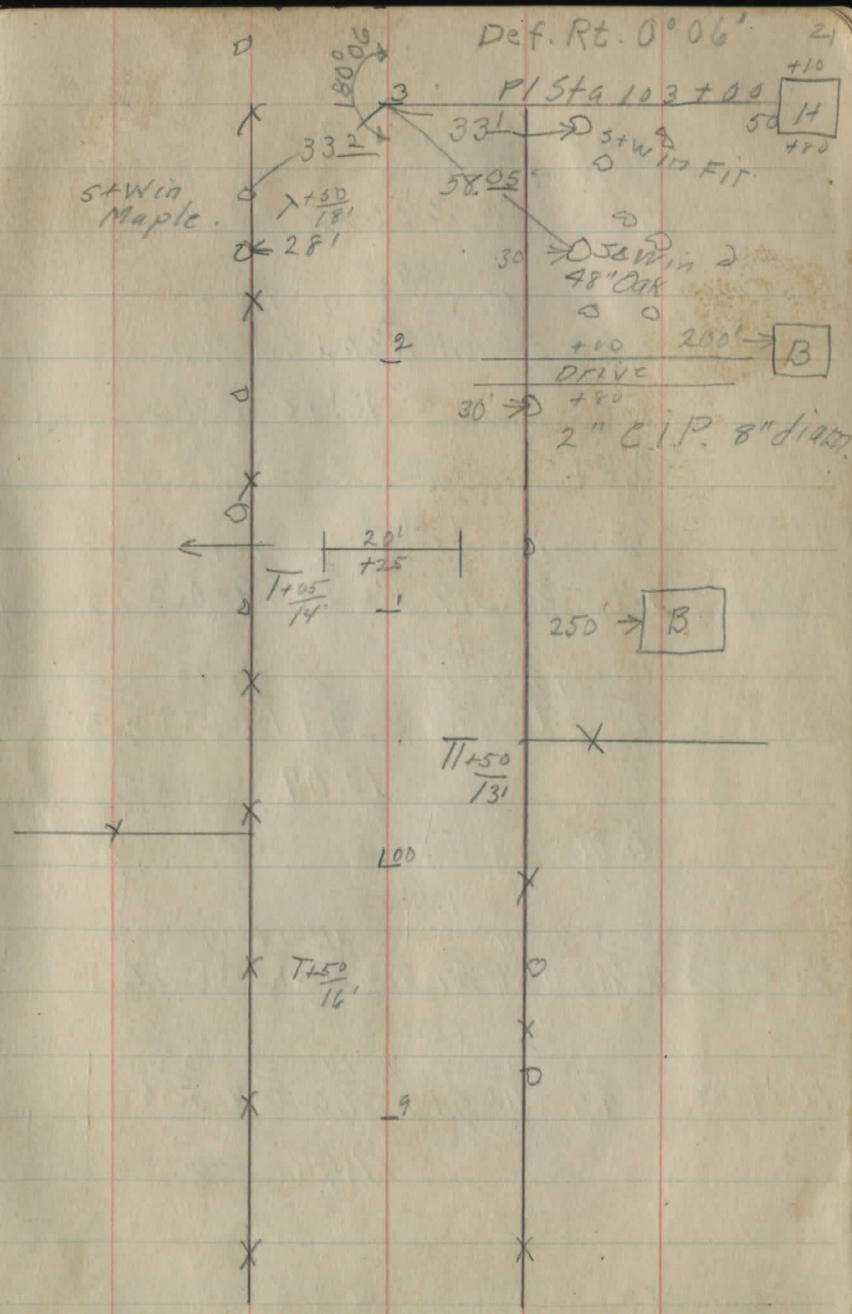
6.52 123.51

5.24 123.75

	25	17	14	5	D	5	15	25			
103+00	4.5	6.2	5.2	4.4	4.4	6.4	9	3.6	3.6		

123.15

BM #9 4.24 123.51 123.42



3.48 1236.99 1232.5

104+00	25 3.7	17 5.0	14 5.8	11 5.0	4 4.3	6 4.5	4 4.8	5 5.5	8 4.6	25 5.0

1227.7

105+00	25 5.0	16 5.3	9 10.1	9 9.3	7 10.1	15 6.1	25 7.0	

12.48 1224.51

0.21 1224.72

1221.5

106+00	25 -3.4	13 -3.4	5 3.7	9 3.2	5 3.7	9 4.9	14 -0.3	25 1.2

1215.5

107+00	25 2.4	11 3.7	6 10.6	4 9.6	6 9.2	8 9.9	9 10.8	19 5.9	25 6.3

13.07 1211.65

0.06 1211.71

1208.5

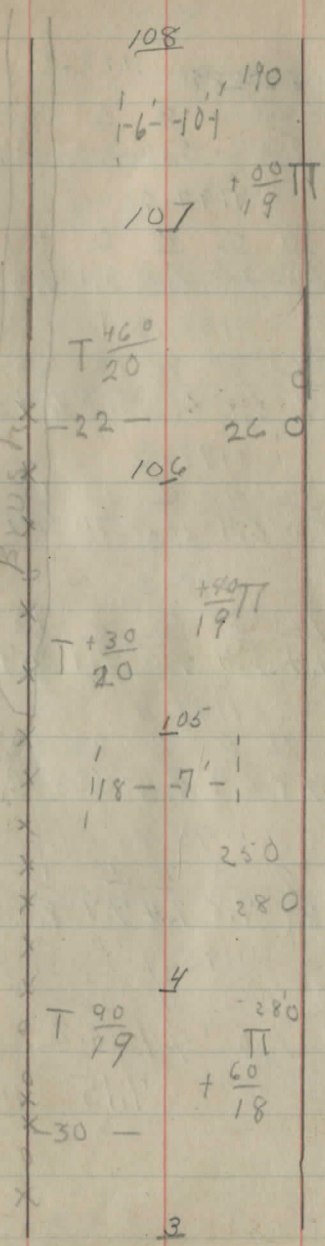
108+00	25 -4.1	21 -4.1	10 2.9	7 4.7	5 3.7	2 3.2	11 9.3	14 4.6	17 3.6	25 4.6

1202.2

109+00	25 9.5	12 11.0	8 9.4	6 9.5	14 9.6	20 12.7	25 12.8	

11.76 1200.25

Temporary BM Sta 110+18 set 7/11/28
NE & E Headwall Elev - 1198.5



2.56 1202.81 1197.8

110+00 25 Q 6 10 21 23
6.5 5.0 4.5 7.9 8.1 5.5

1197.6

110+18 Lip 11.8 5° 10.1 FL 8.7 H 5.2 G 5.6 Q 5.2 G 5.1 H 4.5 EL 8.8

1194.1

1196.5

111+00 25 8 Q 13 23 20 27
8.6 6.6 6.3 5.3 6.4 5.8 4.1

1197.3

112+00 25 13 7 Q 13 16 25
7.8 6.0 6.4 5.5 5.0 5.5 2.8

1198.3

112+60 25 12 6 Q 6 13 25
5.5 4.4 5.4 4.5 4.1 4.7 2.1

1197.3

113+00 25 11 6 Q 12 20 25
5.3 7.8 6.4 5.5 5.8 3.5 3.4

1195.4

117+00 25 12 7 3 Q 10 15 20 25
9.4 8.1 8.9 7.8 7.4 7.9 8.0 6.6 7.1

1195.4

114+30 50 EL Q EL
11.7 10.6 7.4 9.2

1192.8

7.15 1195.66

113

T +30/19

112 +00/18 TT

111

T +90/16. +25/19 TT. 3x3 Conc box FL. Lt good cond

6 17 +18

110

T +45/18

-10-

109

0-22-

+60/18 TT

T +10/18

4.03 1199.69 1195.0

115+00 25 11 9 6 4 9 14 19 25
5.4 5.3 5.8 5.3 4.7 4.7 5.3 4.3 3.6

1194.3

25 11 8 5 4 5 10 11 14 23 25
116+00 5.8 5.7 6.8 6.2 5.4 5.0 5.5 6.0 6.2 4.2 4.0

1194.4

50 FL 4 FL
116+50 9.1 7.8 5.3 7.5

1194.7

1194.3

25 12 10 6 4 5 13 15 18 25
117+00 6.7 6.0 6.9 6.2 5.4 4.9 6.0 6.8 5.9 4.3

1196.0

25 12 7 4 9 12 14 15 19 25
118+00 2.7 2.9 5.0 3.7 3.4 4.4 5.4 4.6 3.5 2.5

1196.9

25 12 8 4 8 15 19 25
118+50 2.8 2.9 4.3 2.8 3.1 4.7 3.1 2.3

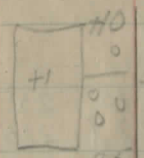
2.59 1199.10

6.82 1197.92 1196.3

25 11 9 4 4 3 11 16 19 25
119+00 1.7 2.2 2.8 2.0 1.6 1.3 2.2 2.8 1.7 1.3

BM

BM #10 1.26 1196.66 1196.55



5+0 118

T +90/16

6 25 25 0

117 +00/19 TT

25 0

T 45/17 5.15 +5.0

116

+30/18 TT

T +12/18

115

19 12

5+12 6" C.I.P.

+30 FL. Lt

114

T +70/17 +60/18 TT

0.78 1197.33 1194.4

120+00	25	13	11	4	8	13	15	25
	1.4	2.0	3.2	2.9	2.9	3.8	2.9	2.6

1191.8

121+00	25	12	7	4	6	10	14	25
	4.0	5.3	5.8	5.5	5.8	6.3	4.8	4.5

1190.8

122+00	25	16	11	7	4	7	10	13	25
	6.8	7.4	8.0	9.3	6.6	7.1	8.0	7.2	7.0

1188.8

123+00	25	13	11	7	4	5	9	13	25
	9.2	9.3	9.8	9.2	8.5	9.0	9.8	8.9	8.8

1187.0

124+00	25			8	7	10	13	25
		10.9	10.3	10.8	11.5	10.6	9.4	

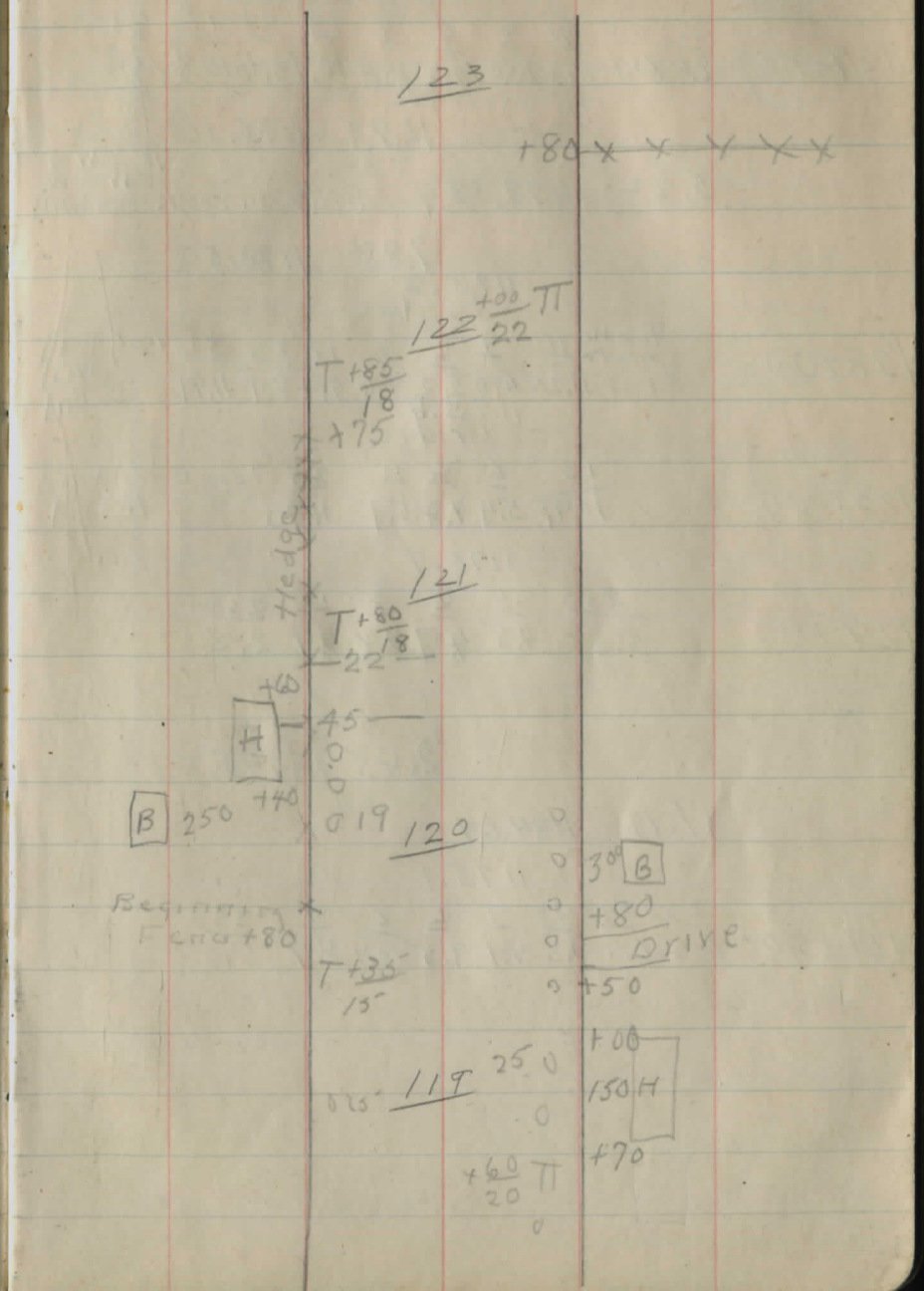
12.14 1185.19

0.70 1185.89 1185.0

125+00	25	13	13	8	2	4	6	10	13	25
	0.2	0.7	1.8	1.5	0.8	0.9	1.3	2.4	0.8	0.00

1181.2

126+00	25	14	12	9	4	4	3	22	25
	2.8	4.6	5.8	5.0	4.4	4.7	5.0	2.0	2.1



1185.9

1175.4

127+00	28	12	10	8	6	4	13	14	17	25
	8.6	10.1	11.3	10.0	10.5	10.4	10.7	11.6	10.8	10.4

12.73 1173.16

15' S.W. of SW cor W.

5.22 1178.38 BM X on rock Headwall

7.88 1170.50

1173.2

Bridge

128+00	Top W. Head Wall	11	3	6	9	17	22	33	Top E Head Wall
	S. End	11.20	6.0	5.2	4.6	5.4	8.1	11.91	S. End

1173.6

Bridge

128+50	13	6	4	11	24	Top E Head Wall	
	10.91	5.4	4.8	5.1	11.70	N. End	

1173.7

129+00	35	5	4	8	12	25
	3.3	4.5	4.7	4.8	4.9	2.2

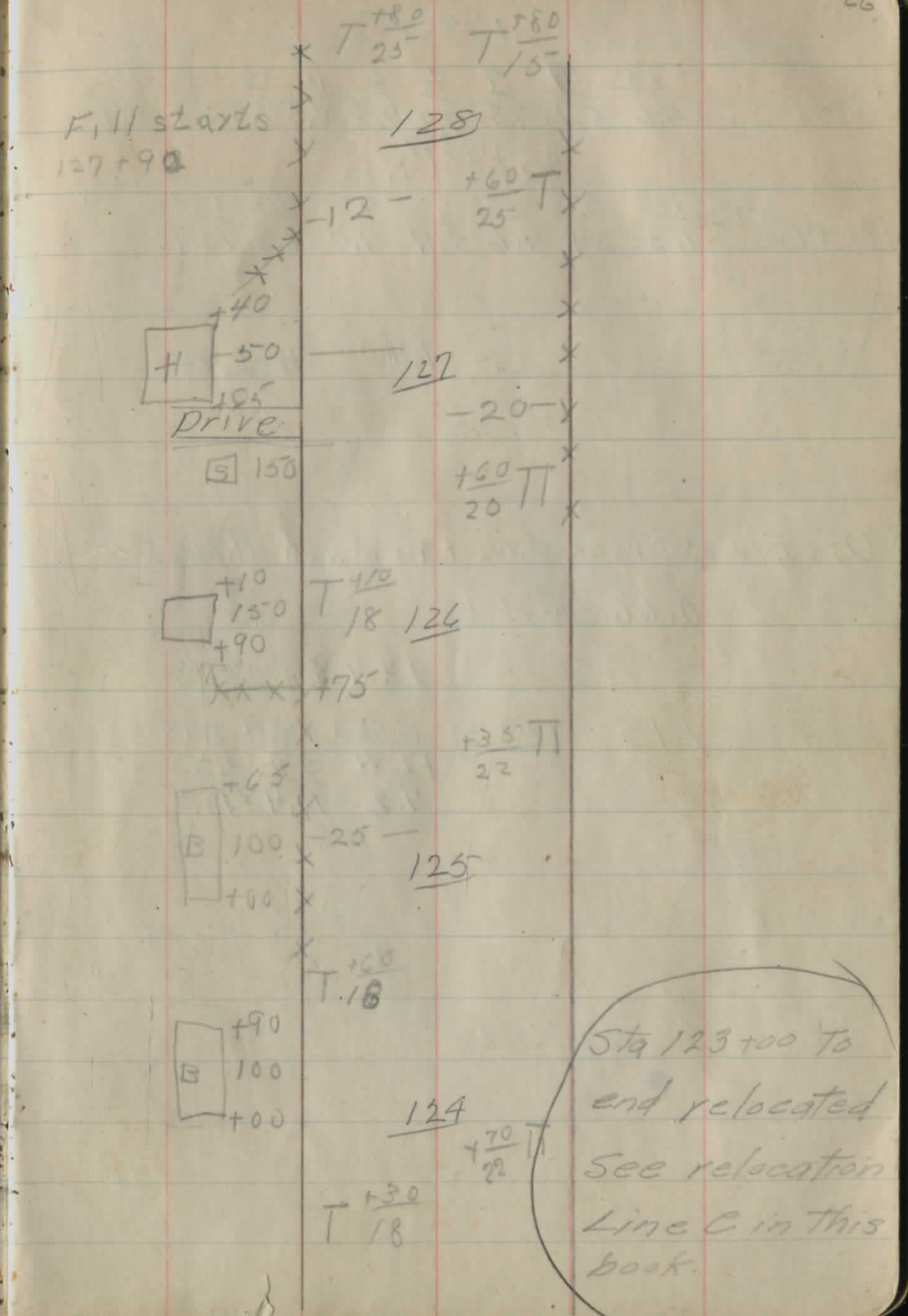
2.85 1175.53

9.11 1184.64

1175.1

129+50	25	23	13	9	4	6	9	23
	6.5	6.9	9.3	9.1	9.5	10.1	8.7	5.10

1162.7



1184.6

1177.4

	25	17	9	5	6	11	13	18	23
130+00	4.6	5.1	7.5	7.2	7.8	8.6	7.5	5.1	4.1

1178.9

Mayfield Rd.

	100	50	25	0	25	50	100
130+40 ℄	1.3	3.7	4.6	5.7	7.0	8.3	10.7

BM #11 1.90 1182.74

Use Elev of rock S.W. of Headwall 1170.50

0.66 1171.16

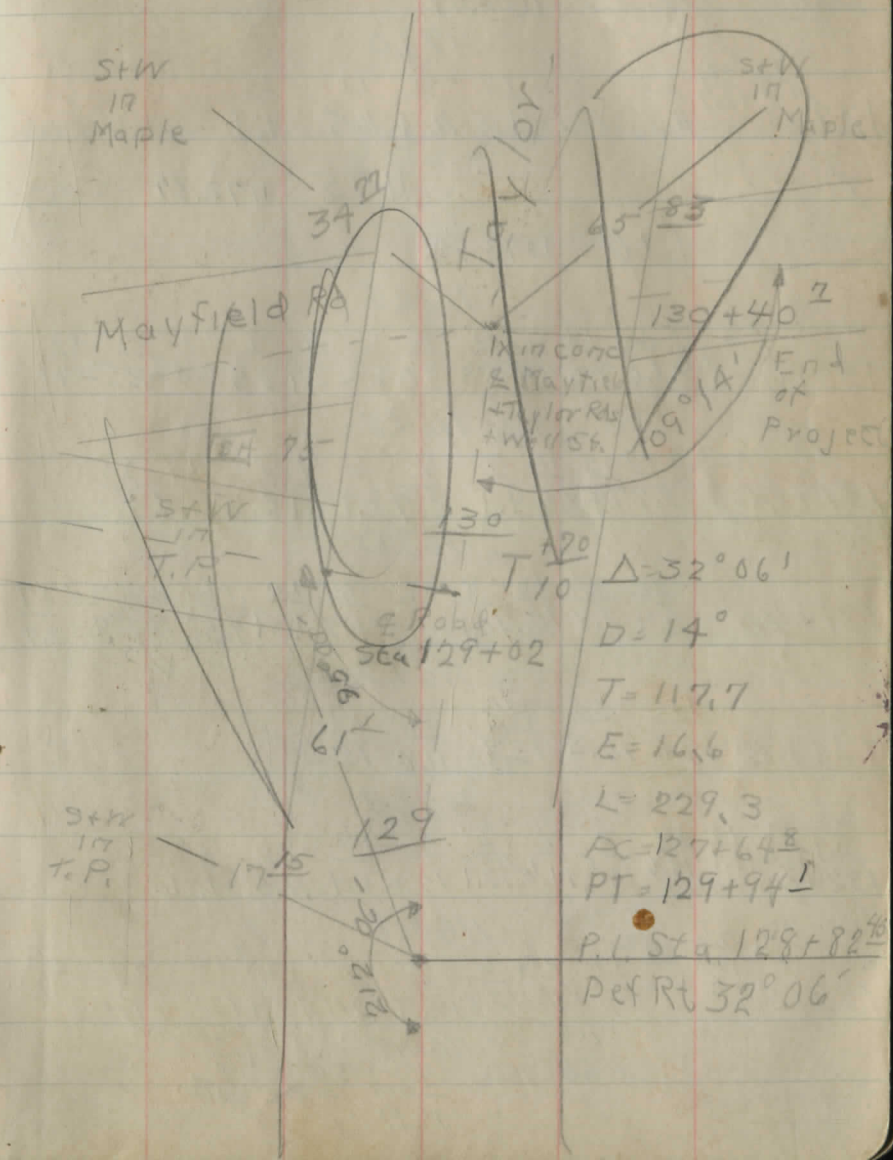
12.98 1158.18

1.13 1159.31 1152.1 1148.9 1148.8

FLW 50 25

7.2 10.4 10.5

all relocation Line C.



Wells St. Y   2/6/28   Richey
Matson
Spohn

1182.74

BM   1.35   1184.09

1173.0

38/14.2 32/12.7 25/11.7 23/12.1 19/11.5 ℄/11.1 21/10.5 25/9.9
129+00

11.75   1172.34

1.16   1173.50

1170.5

35/1.5 25/1.0 20/1.6 14/3.0 9/2.7 4/3.3 ℄/3.0 5/3.2 7/2.7 9/3.0 15/0.0 25/-2.5 32/-4.0
130+00

1164.8

35/5.5 26/5.5 23/6.0 19/5.7 15/7.4 11/8.6 7/9.1 ℄/8.7 6/8.7 9/9.1 12/6.5 19/3.8 25/3.2
131+00

1163.0

30/7.4 20/7.8 12/10.7 8/10.1 ℄/10.5 5/10.3 10/10.7 16/9.5 20/10.5 23/9.3 27/8.9
131+40

1161.9

100/19.6 50/16.3 FL/13.7 ℄/11.6 FL/12.3
131+80.

1161.5

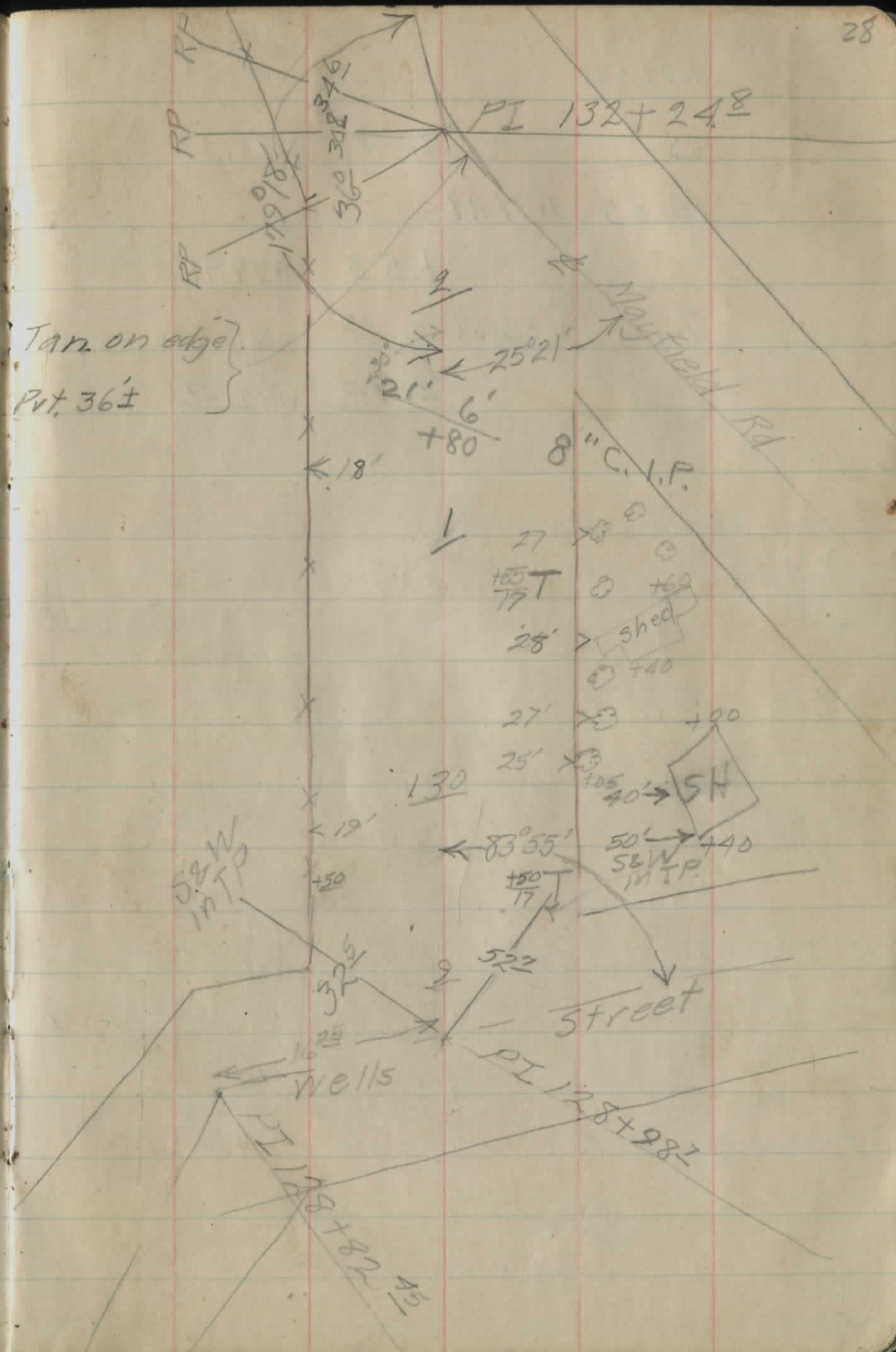
28/11.7 22/12.6 19/12.1 14/15.6 10/12.5 4/11.6 2/12.1 ℄/12.0 10/11.4 20/11.5 25/11.6
132+00

1160.8

30/12.4 25/13.4 19/13.2 14/15.1 8-9/13.5 6/12.8 ℄/12.7 5/12.7 13/12.9 18/13.0 24-25/14.8 32/12.1
132+24.8

1160.8

100/17.6 50/15.0 ℄/12.7 50/8.8 100/6.2
℄ Mayfield



1173.50			1173.50 −4.91 1168.59
		4.91	1168.59
10.85	1179.44		
		1.53	1177.91
7.78	1185.69		
		2.93	1182.56

Line B
Relocation Wells St 3/20/28

B.M 1182.74
Rod 1.98 1184.72

1174.3
130+41 65 — 50/13.3, 25/11.6, ℄/10.4, 25/9.0, 50/7.7

1173.8
130+25 — 25/12.3, ℄/10.9, 25/9.5

1179.6
130+15 & 130 same sect — 25/6.1, ℄/5.1, 25/4.6

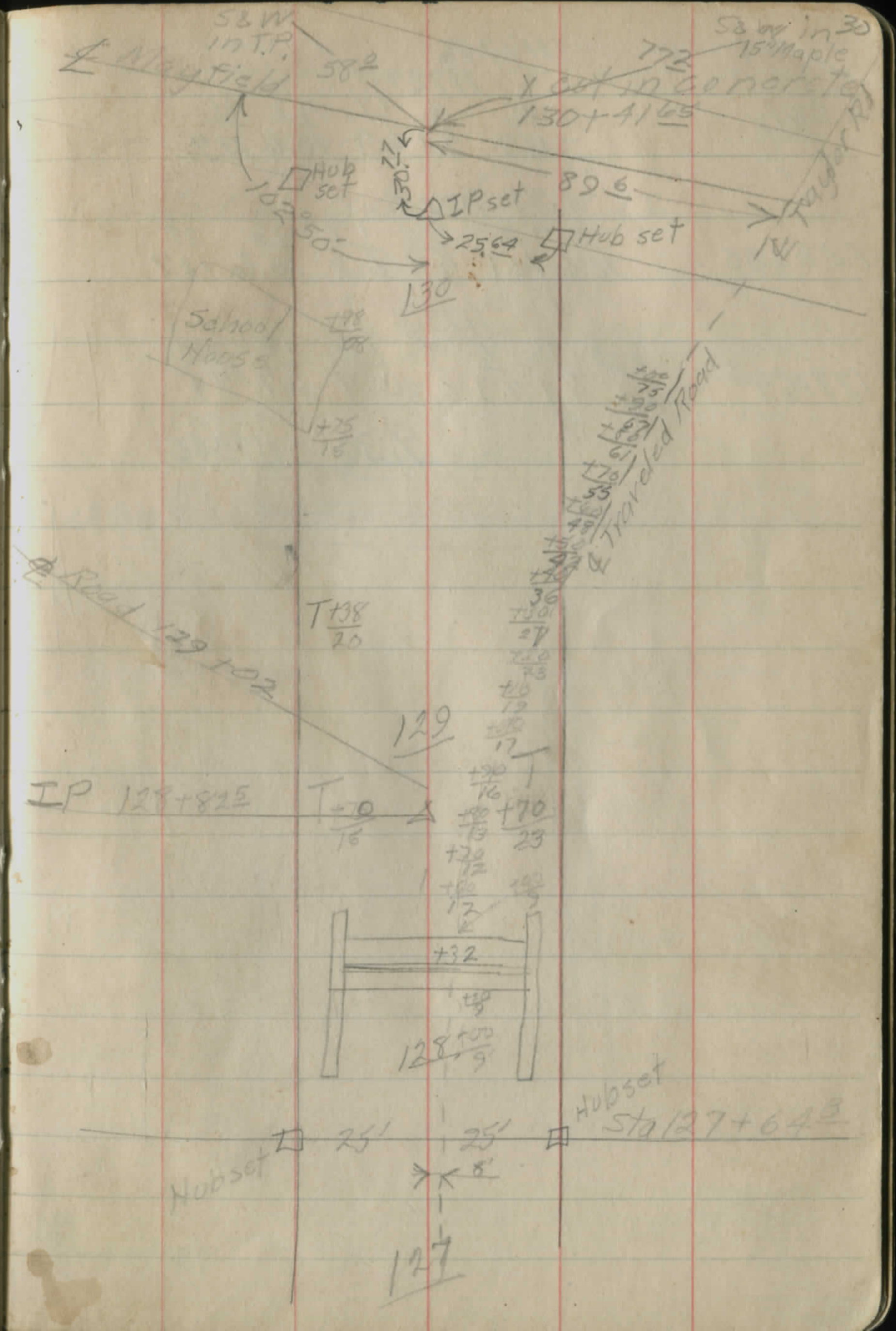
1178.0
129+50 — 25/7.8, ℄/6.7, 15/7.0, 24/9.4, 35/9.2

1174.3
129+30 — 25/12.2, ℄/10.4, 18/9.7, 25/10.2

72.7
129+00 — 27/12.2, 23/13.4, 18/12.1, ℄/12.0, 17/10.8, 25/11.1

1150 1173.22
6.54 1179.76

1171.9
128+65 — 19/15.0, 2/13.4, ℄/7.9, 2/6.7, 17/6.3, 27/10.9, 35/10.5



1179.76

1172.7

℄ Culv. H/12.3 ℄/7.1 17/6.7 23/10.6 H/11.7

1172.8

128+00 8/16.6 -8/12.1 ℄/7.0 19/6.8 26/10.6 30/12.7

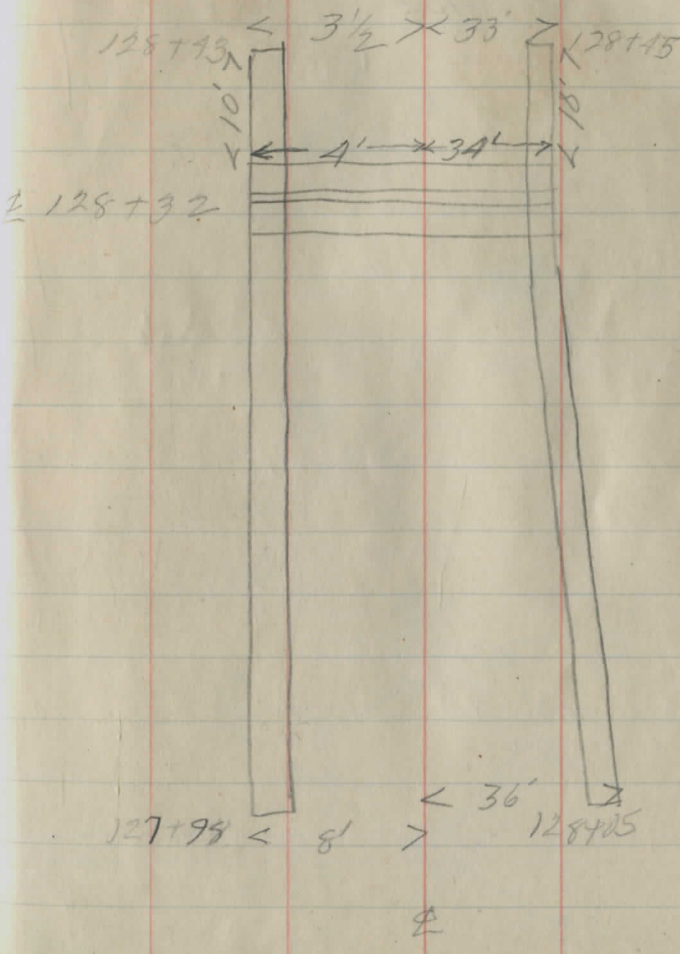
1173.5

127+64.8 23/7.3 11/7.1 6/7.3 ℄/6.3 16/5.9 18/6.7 25/7.4

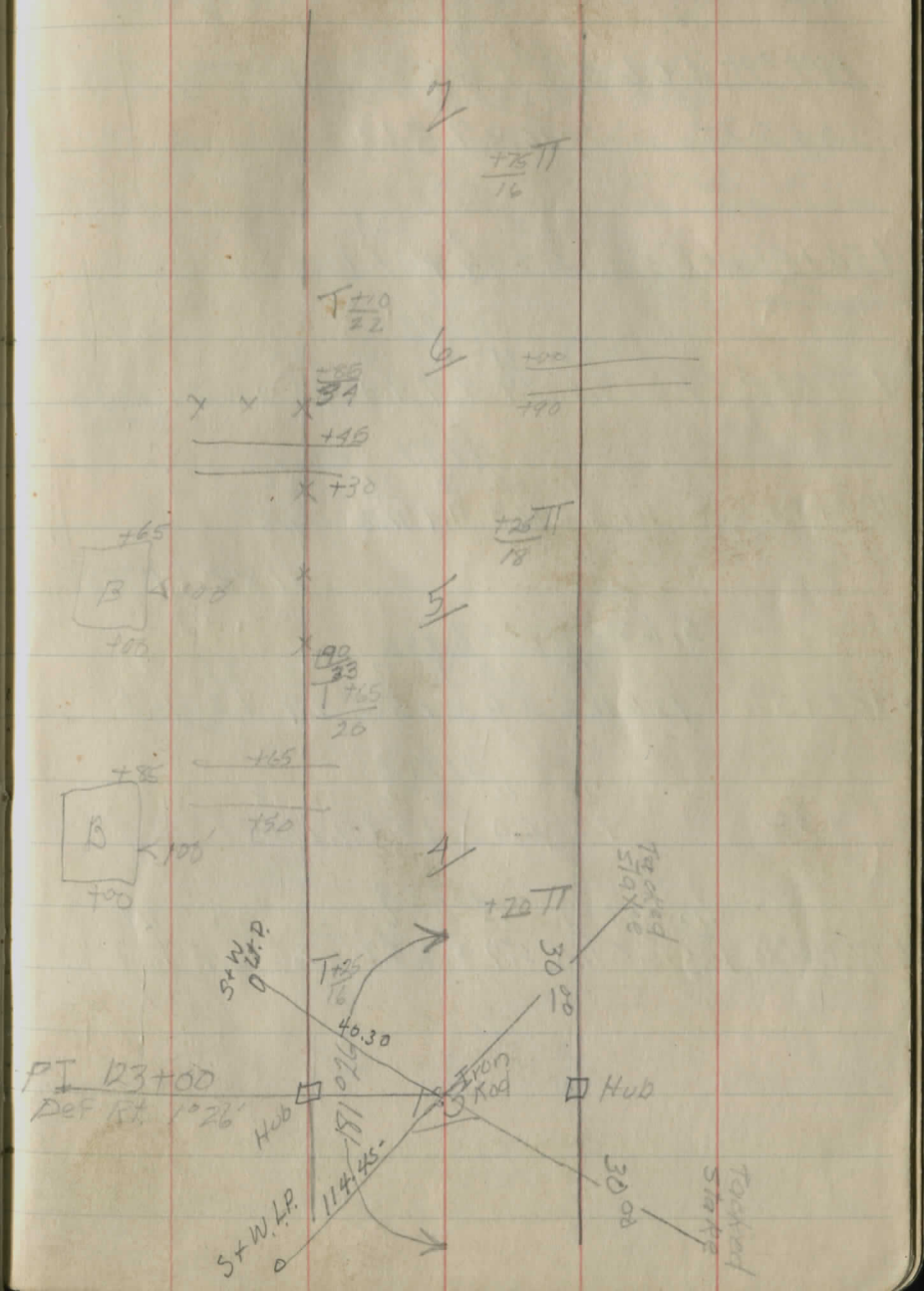
9.30 1170.46

Detail of culvert 128+32

℄



Line C
Wells St Relocation 3/22/28



Line C

1182.71

BM #11 2.86 1184.77 1175.3

25 ℄ 25
10.8 9.5 8.2

130+37.3

1179.9

25 ℄ 23
5.4 4.9 4.9

130+00

1174.9

23 11 ℄ 18 25
7.5 7.9 9.9 9.4 10.0

129+50

1173.7

25 ℄ 21 23
12.3 11.1 11.3 9.8

129+00

TP 11.82 1172.95

5.62 1178.57 1173.5

32 18 19 ℄ 7 14 25 22
13.6 11.2 5.6 5.1 5.5 9.9 9.3 12.6

128+50

1173.3

18 11 ℄ 6 12 18
9.7 6.0 5.3 5.7 9.8 10.5

128+32

1173.4

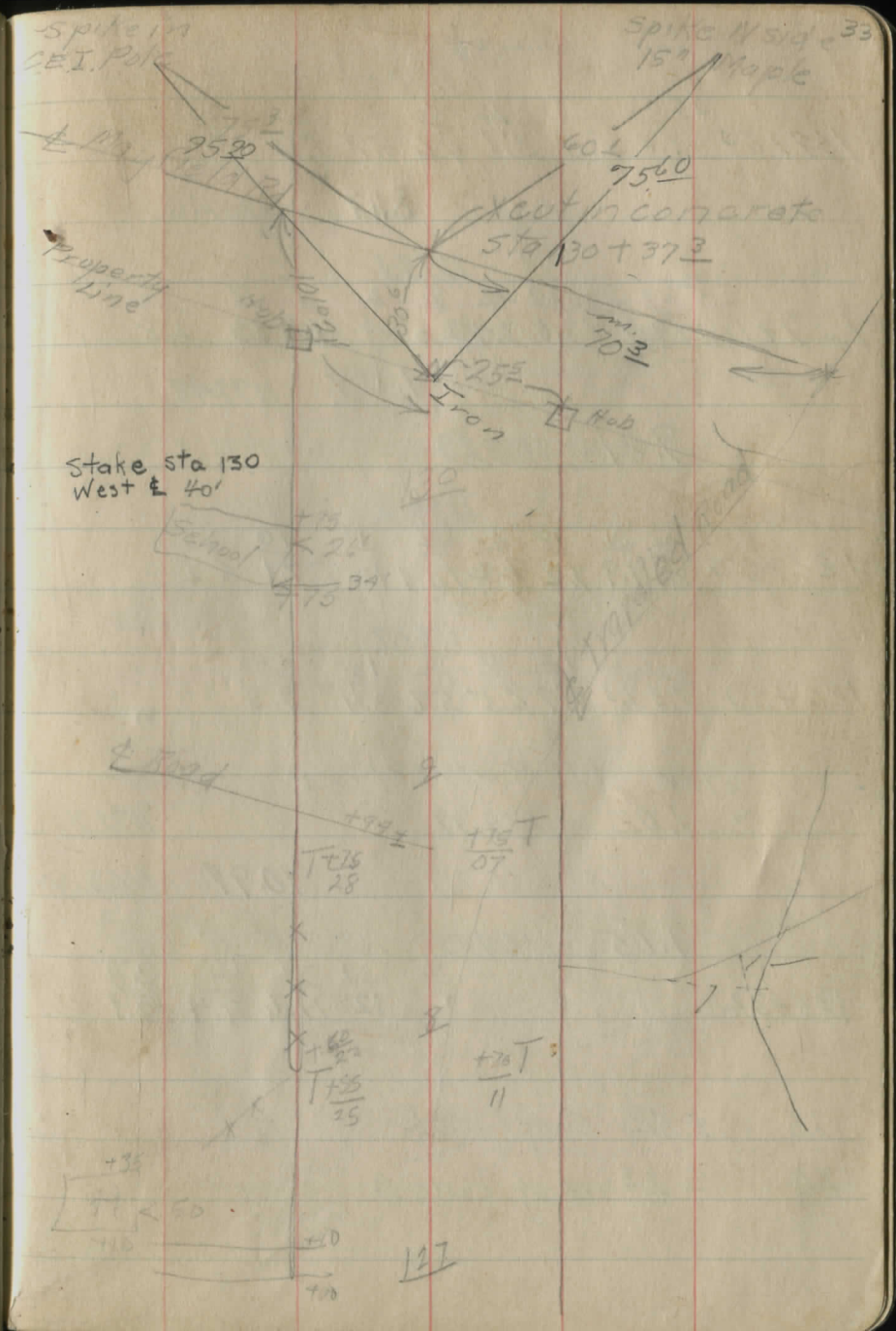
40 21 21 12 ℄ 6 20 30 42
12.9 15.8 11.0 5.7 5.2 5.7 11.6 12.5 13.7

128+00

1174.8

25 ℄ 25
11.5 10.0 8.7

130+25



Line C

1178.57

1174.0

25 22 20 19 4 2 5 25

137+60 6.0 6.3 5.1 4.6 4.2 5.7 8.0

TP 8.17 1170.40

1175.1

25 23 22 20 11 4 2 4 7 25

127+00 2.7 4.3 3.0 3.4 3.6 3.5 4.3 3.5 2.8

TP 1.09 1177.48

9.81 1187.29

1177.2

24 21 18 4 4 1 10 25

125+50 8.2 9.9 9.2 9.2 10.1 10.5 7.1 6.2

1181.7

25 20 12 4 4 13 25

126+00 5.3 7.3 5.9 6.5 5.6 3.4 3.3

Use elev of T.P. at 128+75 ±

→ 1.02 1173.97 1172.95

10.99 1163.00

1.05 1164.05 1152.0 1152.9 1154.6 1154.9

± 12 32 40 30

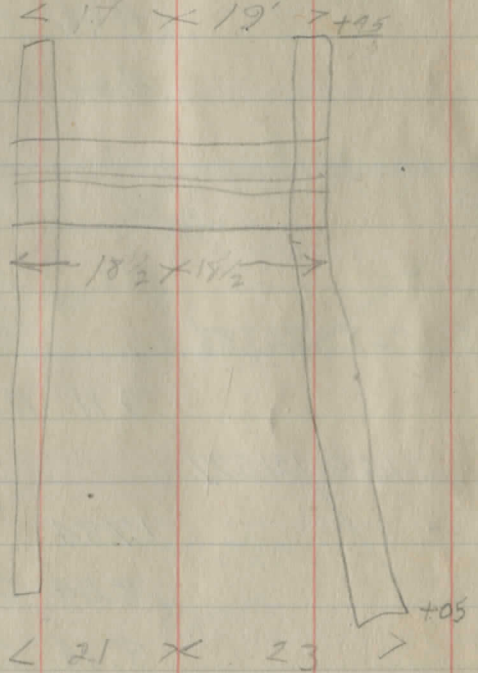
128+32 120 11.6 9.4 9.1

125 ± 5° E of Line A

124 ± 2° E of Line A

130 37

128+34



128

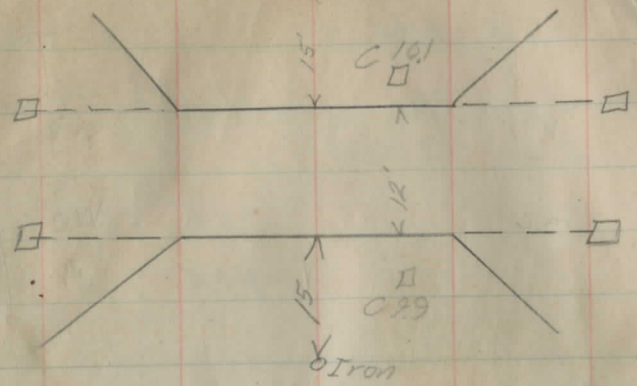
5/21/28 Richey Parks Spohn

	BS	HI	FS	Elev.
BM #1				1201.98
	0.12	1202.10		
			10.76	1191.34
	5.35	1196.69		
Exc. Rod			14.56	1182.13
N			4.46	C10.1
S			4.66	C9.9

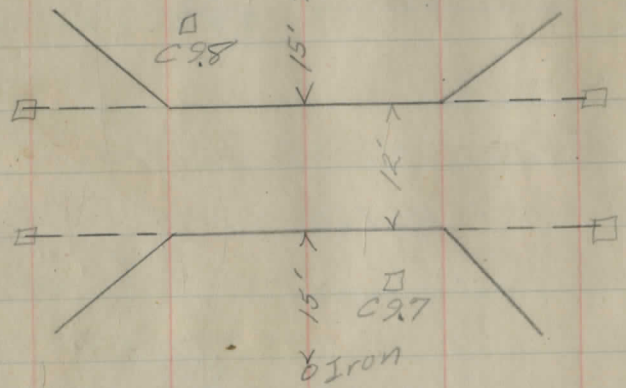
6/9/28 Richey Parks Whiskin Spohn

	BS	HI	FS	Elev
BM #3	5.68	1223.88		1218.20
			9.11	1214.77
	1.20	1215.97		
Grade Rod -			17.84	1198.13
N			8.04	C9.8
S			8.14	C9.7

℄ Iron Sta. 7+67



℄ Iron Sta 33+26

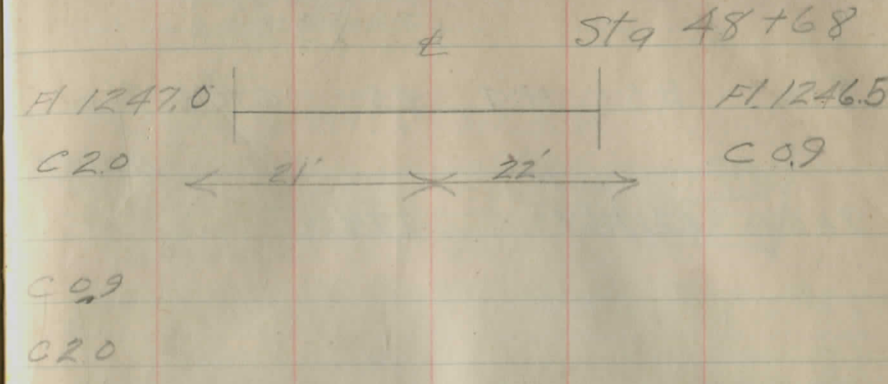


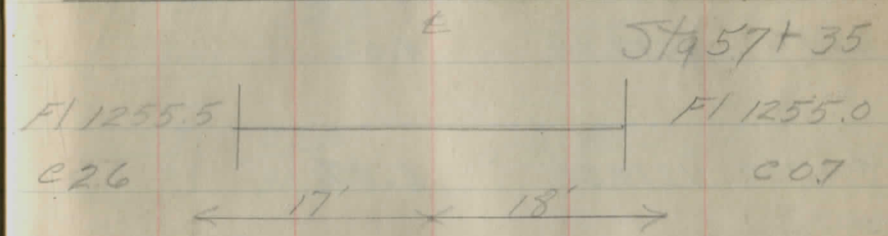
5/31/18 Richey Parks
Whiskin Spolum

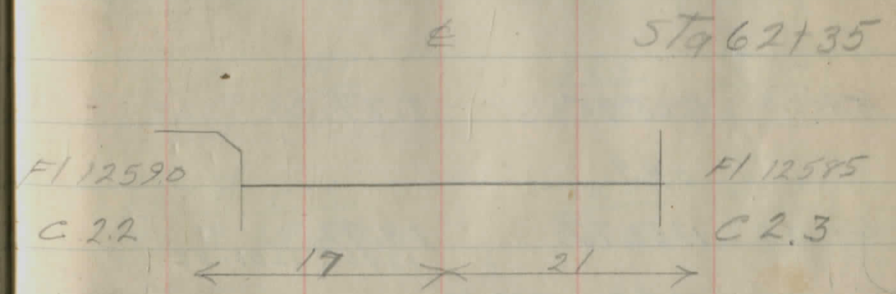
	BS	HI	GradeRod	FS	
BM #5	0.93	1265.15			1264.22
			11.71	1253.44	
	2.60	1256.04			
Flow R			9.54	8.64	1246.5
Flow L			9.04	7.04	1247.0

	BS	HI	GradeRod	FS	
BM #6	0.31	1264.84			1264.53
Flow R			9.84	9.14	1255.0
Flow L			9.34	6.74	1255.5

	BS	HI	GradeRod	FS	
BM #6	3.07	1267.60			1264.53
Flow R			9.10	6.80	1258.5
Flow L			8.60	6.40	1259.0
TP			8.80	1258.80	







Sta	B.S.	H.I	F.S	G Rod	Elev
					1201.98
1+00	1219.67		2.74		
2+00	1218.39		4.02		
3+00	1215.54		6.87		
4+00	1211.14		11.27		
5+00	1205.95		8.74		
	0.49				
6+00	1200.77		13.92 12.86		1201.83
	0.49	1202.32			
7+00	1196.99		5.33		

15' berm
19.3 ditch
23.3 slope

32" = 2'-8" ditch

37

C1.5 / 26.0 | C1.1 / 25.0 | F0.2 / 23.0 | F0.1 / 24.0

Sta 6+50 to 8+50 7' berm

C2.9 / 27.6 | C2.2 / 26.6 | C0.8 / 24.5 | C1.0 / 25.5

C4.9 / 31.8 | C5.0 / 30.8 | C2.8 / 27.6 | C2.9 / 28.5

C6.0 / 33.3 | C6.0 / 32.3 | C3.1 / 28.0 | C3.3 / 29.0

C5.2 / 31.5 | C4.8 / 30.5 | C2.0 / 24.8 | C2.3 / 27.3

C1.9 / 24.7 | C1.6 / 25.7 | C1.5 / 25.6 | C1.3 / 26.6

F6.7 / 29.9 | F7.0 / 28.9 | F8.0 / 30.5 | F7.7 / 31.5

Sta	B.S.	H.I.	F.S.	G. Rod
			11.49	1190.83
	5&5	1199.48		
8+00	1196.00		3.48	
			2.53	1196.95
	8.52	1205.47		
9+00	1197.80		7.67	
10+00	1200.34		5.13	
11+00	1201.57		3.90	
12+00	1202.14		3.33	
13+00	1202.72		2.75	
14+00	1203.29		2.18	
			1.37	1203.10
	4.19	1209.05		1204.86
15+00	1203.86		5.19	

19.3
23.3

F5.0 / 26.3	F5.2 / 25.3	F5.0 / 30.5	F7.8 / 31.5
F2.4 / 22.3	F1.5 / 21.3	C3.2 / 28.4	C3.2 / 29.1
C0.6 / 25.0	C0.4 / 24.0	F0.2 / 23.8	F0.1 / 24.0
C0.2 / 24.3	C0.0 / 23.3	F0.2 / 23.6	F0.1 / 24.0
C0.7 / 24.9	C0.4 / 23.9	C0.1 / 23.5	C0.2 / 24.5
C0.5 / 24.8	C0.3 / 23.8	F0.8 / 22.1	F0.7 / 23.1
F0.4 / 23.5	F0.5 / 22.5	F1.1 / 21.5	F0.9 / 22.5
C0.1 / 24.3	C0.0 / 23.3	F1.2 / 21.5	F1.1 / 22.5

16+00	1204.42	4.63
17+00	1205.00	4.05
18+00	1205.57	3.48
19+00	1206.13	2.92
20+00	1206.78	2.27
21+00	1207.88	1.17
		0.50 1208.46
	8.27 1216.73	
22+00	1209.43	7.30
23+00	1211.04	5.68

19.3
23.3

39

C2.0 / 27.3	C1.9 / 26.2	F1.0 / 21.7	F0.9 / 22.7
C0.0 / 24.1	F0.1 / 23.0	F1.4 / 21.0	F1.5 / 22.0
F1.9 / 22.2	F1.4 / 21.2	F2.0 / 20.3	F1.9 / 21.3
F1.6 / 22.0	F1.5 / 21.0	F2.0 / 20.3	F2.0 / 21.3
F0.1 / 23.8	F0.3 / 22.8	F1.6 / 21.0	F1.5 / 22.0
C1.1 / 25.8	C1.0 / 24.8	F0.8 / 22.3	F0.7 / 23.1
C0.4 / 24.6	C0.2 / 23.6	F0.4 / 22.7	F0.2 / 23.7
C1.0 / 25.5	C0.8 / 24.5	C0.1 / 23.5	C0.3 / 24.5

24+00	1212.69	4.04
25+00	1214.31	2.42
26+00	1215.93	6.45
27+00	1217.56	4.82
28+00	1219.09	3.29
29+00	1219.90	2.48

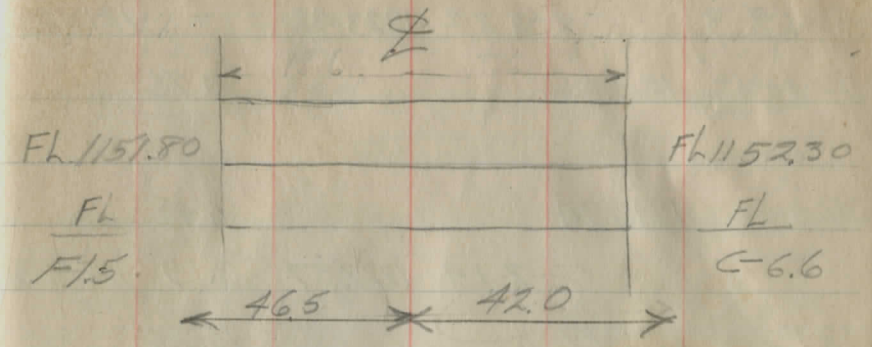
19.3
23.3

C1.7 / 26.4	C1.4 / 25.4	F0.1 / 23.0	C0.0 / 24.0
C1.1 / 25.8	C0.9 / 24.8	C0.1 / 23.5	C0.1 / 24.5
C1.2 / 25.7	C0.9 / 24.7	C0.1 / 23.5	C0.2 / 24.5
C0.1 / 24.6	C0.2 / 23.6	F0.1 / 23.0	C0.1 / 24.0
C0.1 / 24.0	F0.1 / 23.0	C0.1 / 25.5	C0.3 / 24.5
F0.9 / 22.6	F1.1 / 21.6	F0.4 / 22.7	F0.1 / 23.7

7/11/28 — Richey, Whisman, Spohn

Sta.	B.S.	H.I.	F.S.	Elev.	B.M.#11 Sta 130+71 1182.71
	0.01	1182.72			
	3.49	1177.10	9.11	1173.61	
	0.66	1165.56	12.20	1164.90	
	0.63	1156.79	9.40	1156.16	
L off			4.99		1151.80
L Stake			6.49	F1.5	
	1.06	1164.68	3.17	1153.62	
Right			12.38		1152.30
R. Stake			5.78	C6.6	
	10.38	1175.01	0.05	1164.63	
	10.51	1184.22	1.30	1173.71	
B.M.#11			1.50	1182.72	1182.71

Sta. 128+34



Sta	6/19/28	BS	Richey Whaskin HI	Parks Spohn FS	
BM 43		5.22	1223.42		1218.20
30+00	1219.66			3.76	
31+00	1216.94			6.48	
		2.14	1222.37	3.19	1220.23
32+00	1212.17			10.20	
		5.42	1214.91	12.88	1209.49
33+00	1209.30			5.61	
34+00	1208.98			5.93	
35+00	1211.22			3.69	
		1259	1225.23	2.27	1212.64
36+00	1215.99			9.24	
		13.02	1237.34	0.91	1224.32
37+00	1223.00			2.23	
38+00	1230.33			7.01	
		1227	1249.55	0.06	1237.28

	F0.5 / 23.3	F0.7 / 22.8	C0.1 / 23.5	C0.4 / 24.5
	C3.3 / 29.1	C3.2 / 28.1	C3.0 / 27.8	C3.3 / 28.8
	C4.0 / 29.9	C3.7 / 28.9	C2.5 / 27.0	C2.9 / 27.0
7' Berms	F4.1 / 24.1	F4.1 / 23.1	F4.8 / 24.5	F4.8 / 25.5
7' Berms	F3.2 / 22.3	F3.2 / 21.3	F3.1 / 21.7	F3.0 / 22.1
7' Berms	F1.1 / 23.4	F1.3 / 22.4	F1.2 / 22.5	F1.1 / 23.5
7' Berms	F2.5 / 21.5	F2.8 / 20.5	F2.5 / 20.6	F2.4 / 21.6
7' Berms	F3.8 / 23.2	F4.0 / 22.9	F4.- / 24.1	F4.6 / 25.1
	C5.5 / 32.4	C5.4 / 31.4	C2.1 / 26.4	C2.8 / 27.4

Sta		BS	HI	FS	
			124.55		
39+00	1237.47			12.08	
BM #4		0.26	124.65	0.26	124.29
40+00	1243.20			6.45	
BM #4		2.38	125.77		124.39
41+50	1247.34			4.43	
42+00	1250.09			1.68	
		9.71	1259.14	2.34	1249.43
43+00	1252.63			6.51	
44+00	1255.19			3.95	
		11.21	1265.17	5.18	1253.96
45+00	1256.92			8.25	
46+00	1257.05			8.12	
BM #5				0.96	1264.21
47+00	1255.57			9.60	
		3.03	1256.61	11.59	1253.58

	C7.8 / 34.9	C7.1 / 33.9	C4.6 / 30.2	C3.7 / 31.2
124.39				
	C4.8 / 31.2	C4.6 / 30.2	C2.6 / 27.2	C2.9 / 28.2
	C2.1 / 27.1	C1.9 / 26.1	F1.8 / 20.6	F1.5 / 21.6
	F2.2 / 26.6	F2.5 / 20.6	F4.9 / 23.7	F4.7 / 24.7
	C2.8 / 38.0	C2.5 / 27.0	C0.5 / 24.0	C1.0 / 25.0
	C0.6 / 24.7	C0.3 / 23.7	F1.2 / 21.5	F1.3 / 22.5
	F1.1 / 22.2	F1.4 / 21.2	C0.0 / 23.3	F0.1 / 24.3
Summit section	C6.2 / 25.8	C6.0 / 24.8	C2.8 / 20.7	C3.2 / 21.4
126.22				
	C1.8 / 26.8	C1.7 / 25.8	F2.1 / 20.2	F2.1 / 21.2

		BS	HI	FS	
			1256.61		
48+00	1253.94			2.67	
49+00	1253.65			2.96	
		12.02	1265.43	3.20	1253.41
50+00	1254.66			10.77	
51+00	1257.00			8.43	
52+00	1260.00			5.43	
53+00	1261.95			3.48	
54+00	1261.80			3.63	
		4.46	1265.15	4.74	1260.69
55+00	1260.60			4.55	
56+00	1259.40			5.75	
57+00	1258.54			6.61	
		8.84	1265.97	8.02	1257.13

7' Berm	F2.9 / 21.9	F3.0 / 20.9	F2.8 / 30.5	F8.2 / 31.5
7' Berm	F4.1 / 24.3	F4.2 / 23.3	F3.2 / 21.3	F3.1 / 22.3
	C3.8 / 29.1	C3.2 / 28.1	C1.5 / 25.5	C1.5 / 26.5
	C7.2 / 34.6	C6.9 / 33.6	C2.1 / 26.4	C2.2 / 27.4
	C3.2 / 28.2	C3.3 / 27.2	C1.1 / 24.9	C1.2 / 25.9
Summit Section	C0.5 / 17.0	C0.2 / 16.0	F0.2 / 15.5	F0.1 / 16.5
	C2.4 / 27.3	C2.0 / 26.3	F1.3 / 21.4	F1.1 / 22.4
	F0.3 / 23.3	F0.7 / 22.3	F1.9 / 20.5	F1.6 / 21.5
	F0.8 / 22.7	F1.1 / 21.7	F3.0 / 19.9	F2.9 / 20.9
	F1.5 / 21.9	F1.6 / 21.9	F3.0 / 19.9	F2.8 / 20.9

		BS	HI	FS		
			126.97			
58+00	125.44			7.53		
59+00	125.01			6.96		
60+00	126.33			5.64		
BM #6				1.47	126.50	126.53

F1.1 / 22.2	F1.4 / 21.2	F2.1 / 20.2	F2.0 / 21.2
F0.3 / 23.4	F0.6 / 22.4	F2.2 / 20.0	F2.1 / 21.0
F0.4 / 23.3	F0.7 / 22.3	F2.4 / 19.7	F2.3 / 20.7

6/18/28

Richey Whiskin · Parks Spohn {Rachna Flint

Sta	6/18/28	BS	HI	FS							
BM #6		1.62	1266.15		1264.53						
61+00	1261.41			4.74			C2.4 / 27.4	C2.1 / 26.4		C0.4 / 23.9	C0.7 / 24.9
62+00	1261.30			4.85		special	C0.7 / 24.2	C0.6 / 23.2		F0.4 / 24.6	F0.2 / 25.6
63+00	1260.60			5.55		special	F1.6 / 21.5	F1.7 / 20.5		F1.6 / 25.7	F1.6 / 26.7
64+00	1259.90			6.25		Special	F0.7 / 20.9	F1.2 / 20.9		F1.9 / 21.4	F1.6 / 22.4
		4.21	1263.16	7.20	1258.95						
65+00	1259.20			3.96			F1.2 / 22.2	F1.4 / 21.2		F1.9 / 20.5	F1.9 / 21.5
66+00	1258.80			4.36			F1.4 / 21.6	F1.8 / 20.6		F1.7 / 20.8	F1.7 / 21.8
67+00	1259.00			4.16			F1.4 / 22.1	F1.5 / 21.1		F1.9 / 20.5	F1.8 / 21.5
68+00	1259.50			3.66			F0.8 / 23.0	F0.9 / 22.0		F1.6 / 20.9	F1.5 / 21.9
				4.45	1258.71						
69+00	1260.54						—	24.8		22.8	—

	7/12/28		Richey Whitkin	Parks Spahn	
STA		BS	HI	FS	
		9.71	1268.42		1258.71
69+00	1260.54			7.88	
70+00	1262.67			5.75	
71+00	1265.33			3.09	
		8.95	1274.30	3.07	1265.35
72+00	1267.48			6.82	
73+00	1268.60			5.70	
74+00	1269.20			5.10	
		6.90	1276.48	4.72	1269.58
BM #7				1.94	1274.58
75+00	1269.80			6.68	
76+00	1270.88			5.60	
77+00	1272.92			3.56	
78+00	1275.93			0.55	

C1.2 / 25.6	C0.9 / 24.6	C0.0 / 23.3	C0.2 / 24.3	
C2.1 / 26.8	C1.7 / 25.8	C0.2 / 23.6	C0.2 / 24.6	
C3.0 / 28.9	C3.1 / 27.9	F0.4 / 22.7	F0.4 / 23.7	
C2.6 / 27.6	C2.2 / 26.6	C0.6 / 24.2	C0.6 / 25.2	
C3.3 / 28.9	C3.1 / 27.9	C2.3 / 26.7	C2.3 / 27.7	
C4.5 / 30.6	C4.2 / 29.6	C2.6 / 27.2	C2.6 / 28.2	
				127.457
C0.5 / 24.3	C0.0 / 23.3	F2.4 / 19.7	F2.2 / 20.7	
F2.4 / 20.6	F2.5 / 19.6	F3.1 / 20.1	F3.0 / 21.1	
C0.5 / 25.2	C0.6 / 24.2	F1.3 / 21.4	F1.1 / 22.4	
F0.5 / 22.8	F1.0 / 21.8	F1.7 / 20.8	F1.7 / 21.8	

Sta		BS	HI 127648	FS						
		11.47	128688	1.07	1275.41					
79+00	127987			6.99		F2.0 / 21.0	F2.2 / 20.0		F2.8 / 19.5	F2.6 / 20.5
80+00	128408			2.80		F1.6 / 21.3	F2.0 / 20.3		F1.2 / 21.5	F0.8 / 22.5
		6.88	129265	1.11	1285.77					
81+00	128646			6.19		C1.3 / 18.5	C1.2 / 17.5	Summit Sec	C0.7 / 16.8	C1.0 / 17.8
82+00	128680			5.85		C2.0 / 19.5	C1.8 / 18.5	Summit Sec	C1.4 / 17.8	C1.6 / 18.8
83+00	128508			7.57		C1.8 / 26.5	C1.5 / 25.5		C2.4 / 26.9	C2.3 / 27.9
84+00	128156			11.09		C3.0 / 28.6	C2.9 / 27.6		C3.5 / 28.5	C3.7 / 29.5
		3.19	128306	12.78	1279.87					
85+00	127780			5.26		C2.3 / 27.7	C2.3 / 26.3		C3.0 / 27.8	C2.6 / 28.8
86+00	127404			2.02		C0.5 / 24.9	C0.4 / 23.9		C1.4 / 26.4	C1.5 / 26.4
87+00	127028			12.78		F0.2 / 24.2	F0.1 / 23.2		F0.1 / 23.2	C0.1 / 24.2
		1.39	1172.58	11.87	1171.19					
88+00	126652			6.06		C0.9 / 25.3	C0.7 / 24.3		C1.6 / 25.6	C1.8 / 26.4

Sta		BS	HI	FS	
			1172.58		
89+00	1262.76			9.82	
90+00	1259.00			13.58	
		1.44	1261.35	12.67	1259.91
		4.70	1261.44	4.70	1256.65
91+00	1255.24			6.20	
92+00	1251.48			9.96	
		0.37	1249.76	12.05	1249.39
93+00	1247.72			2.04	
94+00	1244.32			5.44	
95+00	1241.65			8.11	
96+00	1239.70			10.06	
		0.82	1240.74	9.84	1239.92
97+00	1238.48			2.26	
98+00	1237.62			3.12	

F0.4 / 23.4	F0.6 / 22.4	C1.8 / 26.0	C2.3 / 27.0
F0.8 / 23.4	F0.6 / 22.4	C2.0 / 26.3	C2.4 / 27.3
1156.74			
C0.6 / 25.3	C0.7 / 24.3	C1.5 / 25.5	C1.9 / 26.5
F0.6 / 23.3	F0.7 / 22.3	F2.0 / 20.3	F1.7 / 21.3
F2.0 / 21.2	F2.1 / 20.2	F0.4 / 22.7	F0.1 / 23.7
F0.3 / 23.7	F0.4 / 22.7	C1.7 / 25.8	C1.9 / 26.8
C1.3 / 26.2	C1.3 / 25.2	C3.1 / 27.9	C3.3 / 28.2
C0.4 / 24.6	C0.2 / 23.6	C2.4 / 26.9	C2.7 / 27.9
F0.8 / 22.8	F1.0 / 21.8	C0.5 / 24.0	C0.7 / 25.0
F1.4 / 22.1	F1.5 / 21.1	F0.8 / 22.1	F0.6 / 23.1

Sta		BS	HI	FS						
			124.74							
99+00	123.76			3.98		F1.7 / 21.3	F2.0 / 20.3		F1.2 / 21.5	F1.1 / 22.5
100+00	123.90			4.84		F3.1 / 21.5	F3.3 / 20.5		F1.8 / 20.6	F1.8 / 21.6
		4.67	123.760	7.81	1232.93					
101+00	123.96			2.54		F3.6 / 22.5	F3.8 / 21.5		F2.8 / 19.5	F2.5 / 20.5
102+00	123.420			3.40		F3.7 / 23.1	F4.1 / 22.1		F2.5 / 19.6	F2.4 / 20.6
103+00	123.335			4.25		F0.1 / 23.6	F0.5 / 22.6		C0.6 / 24.2	C0.8 / 25.2
BM #9		4.20	123.762	4.20	1233.40	1233.42				
104+00	123.176			5.86		C1.1 / 25.6	C0.9 / 24.6		C0.0 / 23.3	C0.2 / 24.3
BM #9		2.88	123.630		1233.42					
105+00	122.870			7.60		C3.1 / 28.3	C2.7 / 27.3		C1.1 / 24.9	C1.1 / 25.9
106+00	122.418			12.12		C7.0 / 34.0	C6.5 / 33.0		C0.0 / 23.3	F0.1 / 24.3
		2.50	122.574	13.06	1223.24					
107+00	121.819			7.55		C5.5 / 32.1	C5.2 / 31.1		C0.2 / 23.6	C0.4 / 24.6
TPRight →				7.17	1218.57					
108+00	121.146					—	29.0		21.0	—

7/17/28

Richey
Parks
Spohn

sta		BS	HI	FS	
TP		1.68	1220.25		1218.57
108+00	1211.46			8.79	
		1.39	1209.51	12.13	1208.12
109+00	1205.00			4.51	
Temp BM		4.49	1202.64	11.34	1198.17
110+00	1200.41			2.23	
Temp BM					
111+00	1197.97			4.67	
		5.38	1202.54	5.48	1197.16
112+00	1197.40			5.14	
113+00	1197.10			5.44	
114+00	1196.80			5.74	
115+00	1196.50			6.04	
		4.89	1199.09	8.34	1194.20
116+00	1196.30			2.79	

C5.3 / 32.4	C5.4 / 31.4	F3.9 / 21.7	F3.9 / 22.7
F3.6 / 23.7	F4.4 / 22.7	F6.2 / 26.3	F5.8 / 27.3
1198.15			
F4.4 / 23.9	F4.5 / 22.9	F4.8 / 23.6	F3.3 / 24.6
1198.15			
F3.8 / 22.5	F3.8 / 21.5	F1.3 / 21.4	F1.7 / 22.4
F2.3 / 20.7	F2.4 / 19.7	C2.6 / 27.2	C2.7 / 28.2
C0.3 / 24.6	C0.2 / 23.6	C2.3 / 26.7	C2.5 / 27.7
F3.4 / 21.7	F3.4 / 20.7	F1.3 / 21.4	F1.3 / 22.4
F2.3 / 20.7	F2.4 / 19.7	F0.5 / 22.6	F0.5 / 23.6
F2.4 / 20.5	F2.6 / 19.5	F1.0 / 21.8	F0.8 / 22.8

Sta		BS	HI	FS	
			1199.09		
117+00	1195.90			3.19	
118+00	1195.60			3.49	
119+00	1195.30			3.79	
311+10		0.69	1197.24	2.53	1196.56
120+00	1194.52			2.72	
121+00	1192.80			4.44	
122+00	1190.60			6.64	
123+00	1188.40			8.84	
		2.32	1190.61	8.95	1188.29
124+00	1186.20			4.41	
125+00	1183.72			6.89	

F2.6 / 20.5	F2.8 / 19.5	F1.2 / 21.5	F1.1 / 22.5
C1.4 / 26.2	C1.3 / 25.2	C1.7 / 25.8	C2.3 / 26.8
C0.6 / 25.3	C0.7 / 24.3	C1.3 / 26.2	C1.7 / 26.2
1196.55			
C1.6 / 26.4	C1.4 / 25.4	C0.5 / 24.0	C0.7 / 25.0
set but not graded / 24.6	C0.2 / 23.6	F0.3 / 23.7	C0.0 / 24.7
C0.0 / 24.0	F0.2 / 23.0	F0.5 / 22.6	F0.1 / 23.6
F0.2 / 23.6	F0.5 / 22.6	C0.5 / 24.0	C0.5 / 25.0
C0.2 / 24.3	C0.0 / 23.3	C2.1 / 26.4	C2.4 / 27.4
C1.8 / 26.5	C1.5 / 25.5	C3.4 / 28.4	C3.8 / 29.4

Sta	BS	HI	FS					
		1190.61						
126+00	1180.67		9.94		C1.7 / 26.2	C1.3 / 25.2	C3.4 / 28.4	C3.4 / 27.4
	0.04	1178.53	12.12	1178.49				
127+00	1177.49		1.04		F1.6 / 22.0	F1.6 / 21.0	F1.9 / 20.5	F1.8 / 21.5
128+00	1175.46		3.07		F11.8 / 34.8	F12.2 / 33.8	F10.0 / 30.3	F10.0 / 31.3
129+00	1174.71		3.82		F1.5 / 21.8	F1.7 / 20.8	F0.2 / 23.0	C0.3 / 24.0
	10.80	1184.21	5.12	1173.41				
130+00	1173.10		9.11		C4.1 / 30.3	C4.0 / 29.3	C4.6 / 30.2	C4.6 / 31.2
BM #11			1.48	1182.73	1182.71			
129+00								
+50								
130+00								

5/1/29

	BS	HI	FS	Elev	
BM #1	10.75	1212.43			1201.98
	13.05	1223.24	2.24	1210.19	
0+00			3.84	1219.40	
1			3.57	1219.67	
2			4.85	1218.39	
3			7.70	1215.54	
4			12.10	1211.14	
	2.73	1213.12	12.85	1210.39	
5			7.17	1205.95	
6			12.35	1200.77	
	0.42	1203.19	10.35	1202.77	
BM #1			1.21	1201.98	1201.98
7			6.20	1196.99	
8			7.19	1196.00	

C 1.4 / 26.0

F 0.2 / 24.0

C 2.9 / 27.6

C 1.1 / 25.5

C 4.9 / 31.8

C 2.8 / 28.5

C 6.4 / 33.3

C 3.2 / 29.0

C 5.2 / 31.5

C 1.9 / 27.3

C 1.7 / 26.7

C 2.0 / 26.6

F 6.5 / 29.9

F 7.8 / 31.5

F 5.1 / 26.3

F 7.8 / 31.5

		1203.19		
	6.82	1203.87	6.14	1197.05
9			6.07	1197.80
10			3.53	1200.34
11			2.30	1201.57
12			1.73	1202.14
	4.86	1207.49	1.24	1202.63
13			4.77	1202.72
14			4.20	1203.29
BM #2	2.59	1207.45	2.59	1204.90 / 1204.86
15			3.59	1203.86
16			3.03	1204.42
17			2.45	1205.00
	6.20	1210.10	3.55	1203.90

F2.5 / 22.3	C3.1 / 29.1
C0.5 / 25.0	F0.2 / 24.0
C0.2 / 24.3	C0.0 / 24.0
C0.5 / 24.9	C0.3 / 24.5
C0.5 / 24.8	F0.8 / 23.1
F0.4 / 23.5	F1.1 / 22.5
C0.1 / 24.3	F1.1 / 22.5
C2.0 / 27.3	F1.0 / 22.7
C0.0 / 24.1	F1.7 / 22.0

		1210.10				
18			4.53	1205.57	F1.4 / 22.2	F1.8 / 21.3
19			3.97	1206.13	F1.5 / 22.0	F1.8 / 21.3
20			3.32	1206.78	F0.2 / 23.8	F1.5 / 22.0
21			2.22	1207.88	C1.0 / 25.8	F0.6 / 23.1
22			0.67	1209.43	C0.5 / 24.6	F0.1 / 23.7
	8.54	1218.47	0.17	1209.93		
23			7.41	1211.06	C0.9 / 25.5	C0.3 / 24.5
24			5.78	1212.69	C1.8 / 26.4	C0.0 / 24.0
25			4.16	1214.31	C1.0 / 25.8	C0.1 / 24.5
26			2.54	1215.93	C1.1 / 25.7	C0.4 / 24.5
BM #3	5.33	1223.53	0.26	1218.21	1218.20	

		1223.53				
27			5.27	1217.56	C0.1 / 24.6	C0.2 / 24.0
28			4.94	1219.09	C0.0 / 24.0	C0.3 / 24.5
29			3.63	1219.90	F1.0 / 22.6	C0.0 / 23.7
30			3.87	1219.66	F0.6 / 23.3	C0.4 / 24.5
31			6.59	1216.94	C3.3 / 29.1	C3.2 / 28.8
32			11.36	1212.17	C4.0 / 22.9	C2.7 / 28.0
	2.62	1214.40	11.75	1211.78		
33			5.10	1209.30	F4.1 / 24.1	F4.9 / 25.5
34			5.42	1208.98	F3.0 / 22.3	F2.7 / 22.1
35			3.18	1211.22	F0.7 / 23.4	F0.9 / 23.5

		121440		
36			-1.59	121599
	1096	1225.03	0.33	121407
37			2.03	122300
	12.27	1236.63	0.67	122436
38			6.30	123033
	11.86	1248.26	8.23	123640
39			10.79	123747
40			5.06	124320
	6.55	1252.99	1.82	124644
BM#4	3.64	1253.03	3.64	124935 124939
41			5.69	124734
42			2.94	125009
	12.48	1263.24	2.27	125076
43			10.61	125263
44			8.05	125519

F2.5 / 21.5

F2.4 / 21.6

F3.8 / 23.9

F4.6 / 25.1

C5.7 / 33.3

C1.0 / 27.4

C7.8 / 34.9

C3.7 / 31.2

C4.9 / 31.2

C2.7 / 28.2

C2.0 / 27.1

F1.6 / 21.6

F2.3 / 20.6

F4.6 / 24.7

C2.9 / 28.0

C0.9 / 25.0

C.06 / 24.7

F1.5 / 22.5

I.P.		1263.24			
45			6.32	1256.92	
	5.44	1264.44	4.24	1259.00	
46			7.39	1257.05	
BM 5	0.29	1264.51	0.29	1264.15	1264.22
47			8.94	1255.57	
	3.71	1257.31	10.91	1253.60	
48			3.37	1253.94	
49			3.66	1253.65	
	11.06	1266.89	1.53	1255.78	
50			12.28	1254.56	
51			9.84	1257.00	
52			6.84	1260.00	
Temp. BM	2.89	1266.50	3.23		1263.61
53			4.55	1261.95	
54			4.70	1261.80	

F1.2 / 22.2	C0.1 / 24.3
C6.0 / 25.8	C3.1 / 21.4
C1.9 / 26.8	F2.2 / 21.2
F2.7 / 21.9	F8.1 / 31.5
F3.8 / 24.3	F3.0 / 22.3
C4.0 / 29.1	C1.3 / 26.5
C7.5 / 34.6	C2.2 / 27.4
C3.2 / 28.2	C1.2 / 25.9
C0.8 / 25.3	F0.6 / 23.4
C2.3 / 27.3	F1.1 / 22.4

55		126650	5.90	1260.60		F0.4 / 23.3	F1.7 / 21.5
56			7.10	1259.40		F0.9 / 22.7	F2.8 / 20.9
	6.23	126473	8.00	1258.50			
57			6.19	1258.54		F1.3 / 21.9	F2.5 / 20.9
58			6.29	1258.44		F1.0 / 22.2	F2.3 / 21.2
59			5.72	1259.01		F0.4 / 23.4	F2.2 / 21.0
60			4.40	1260.33		F0.5 / 23.3	F2.3 / 20.7
BM#6	2.14	126667	0.18	126455	1264.53		
61			5.26	1261.41		C2.2 / 27.4	C0.5 / 24.9
62			5.37	1261.30		C0.9 / 24.2	F0.2 / 25.6
63			6.07	1260.60		F1.3 / 21.5	F1.7 / 26.7
64			6.77	1259.90		F1.1 / 20.9	F1.7 / 22.4
	4.52	126331	7.88	1258.79			

		1263.31				
65			4.11	1259.20	F1.7 / 22.2	F1.9 / 21.5
66			4.51	1258.80	F1.5 / 21.6	F1.8 / 21.8
67			4.31	1259.00	F1.5 / 22.1	F1.8 / 21.6
68			3.81	1259.50	F0.6 / 23.0	F1.5 / 21.9
69			2.77	1260.54	C1.2 / 25.6	C0.1 / 24.3
	11.64	1273.39	1.56	1261.75		
70			10.72	1262.67	C2.1 / 26.8	C0.6 / 24.6
71			8.06	1265.33	C2.9 / 28.9	C0.0 / 23.7
72			5.91	1267.48	C2.5 / 27.6	C 0.6 / 25.2
73			4.79	1268.60	C3.3 / 28.9	C2.3 / 27.7
	5.27	1277.18	1.48	1271.91		

		127715		
BM 7		2.61	127457	127457
74		7.98	126920	
75		7.38	126980	
76		6.30	127088	
77		4.26	127292	
	10.95	128468	3.45	127373
78			8.75	127593
79			4.79	127982
80			0.60	128408
	8.14	129082	2.00	128268
81			4.36	128646
82			4.02	128680

C4.4 / 30.6	C2.1 / 28.2
F0.4 / 24.3	F2.2 / 20.7
F2.8 / 20.6	F2.9 / 21.1
C0.8 / 25.5	F1.0 / 22.4
F0.1 / 22.8	F1.5 / 21.8
F1.4 / 21.0	F2.1 / 20.5
F1.4 / 21.3	F0.7 / 22.5
C0.0 / 18.5	C1.3 / 17.8
F1.0 / 19.5	F0.9 / 18.8

		1290.82				
83			5.74	1285.08	C 1.8 / 26.5	C 2.4 / 27.9
84			9.26	1281.56	C 3.0 / 28.3	C 3.7 / 29.5
85			13.02	1277.80	C 2.3 / 27.7	C 2.9 / 28.8
	0.63	1280.73	10.72	1280.10		
86			6.69	1274.04	C 0.6 / 24.9	C 1.6 / 26.4
87			10.45	1270.28	C 0.1 / 24.2	C 0.3 / 24.2
88			2.93 / 14.21	1266.52	C 1.0 / 25.3	C 2.2 / 26.4
	0.23	1268.95	12.01	1268.72		
89			6.19	1262.76	F 0.2 / 23.4	C 2.3 / 27.0
90			9.95	1259.00	F 0.6 / 23.4	C 2.5 / 27.3
91			13.71	1255.24	C 0.7 / 25.1	C 0.9 / 26.5
BM#8	0.36	1257.10	12.10	1256.85	1256.74	
92			5.62	1251.48	F 0.6 / 23.3	F 2.4 / 21.3

5/31/28

Richey Whiskin / Parks Spohn

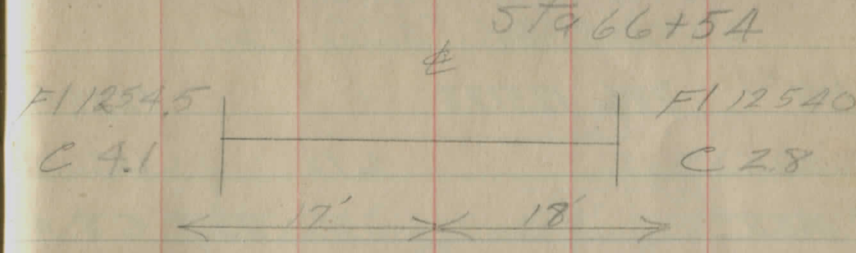
	BS	HI	Grade Rod	FS	
TP				1258.80	
	3.99	1262.79			
Flow R			8.79	5.99	1254.0
Flow L			8.29	4.19	1254.5
			Fl 6.6	100 8.6	

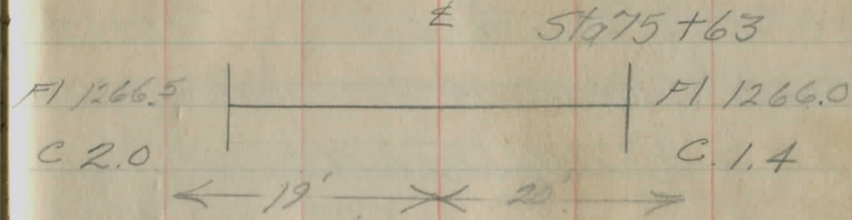
6/20/28

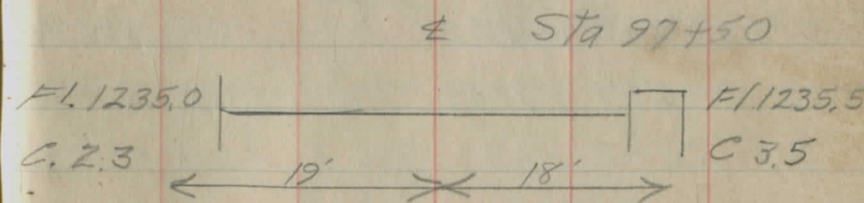
	BS	HI	Grade Rod	FS	Richey Whiskin Parks Spohn
BM#7	1.40	1275.97			1274.57
Flow R			9.97		1266.00
				8.57	C 1.4
Flow L			9.47		1266.50
				7.47	C 2.0

6/20/28

	BS	HI	Grade Rod	FS	
BM#9	4.76	1238.18			1233.42
	7.17	1240.42	4.93	1233.25	
Flow R			4.92		1235.50
				1.42	C 3.5
Flow L			5.42		1235.00
				3.12	C 2.3







7/11/28 — Richey Winship Spohn

	BS	HI	Grade	Stake	
BM #9	3.86	1237.28			1233.42
Flow R			6.78		1230.50
Stake R				3.38	C 3.4
Flow L			7.28		1230.00
Stake L				5.68	C 1.6

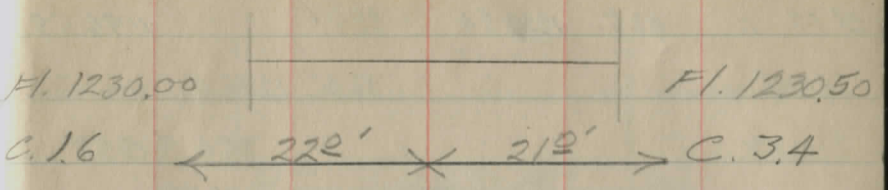
7/11/28

BM #10	4.05	1200.60			1196.55
	7.74	1200.14	8.20	1192.40	
	4.73	1202.29	2.60	1197.54	
Flow R			8.79		1193.50
Stake R				3.29	C 5.5
Flow L			9.29		1193.00
Stake L				6.49	C 2.8

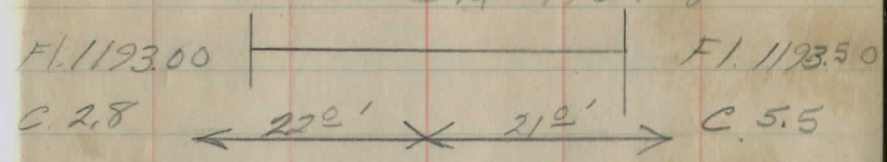
9/10/28

BM #10	4.67	1201.22			1196.55
	5.17	1199.09	7.30	1193.92	
Flow R			6.09		1193.00
Stake R				2.79	C 3.3
Flow L			6.59		1192.50
Stake L				5.89	C 0.7

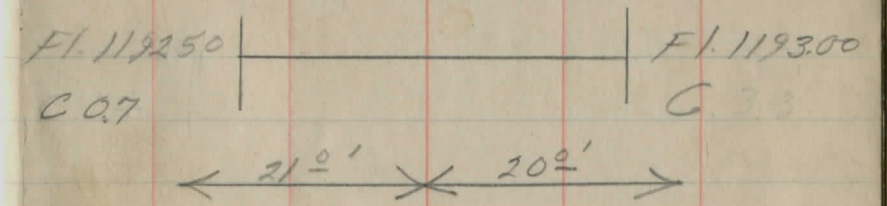
Sta 101 + 25



Sta 110 + 18



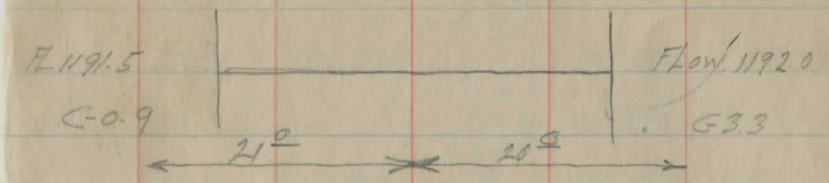
Sta 114 + 30



9/15/28 Whitespin Snyder

	BS.	H.I	Grade	Stake	Elev
B.M. # 10	4.25	1200.80	8.80		1196.55
FL R			8.60	1292.0	
Stake R				350	C 3.3
FL L			9.22		
Stake			9.30	8.40	C 0.9

Sta 116+50



Workman
Spahn
Snyder
10/22/26

Sta		BS	HI	FS				
70+50	1264.00		1266.55	2.55				
71+00	1265.33			1.22	FOS	1264.83	T.P.	
+50	1266.54	8.64	1273.47	6.93				
72+00	1267.48			5.99				
+50	1268.17			5.30				
73+00	1268.60			4.87				
+50	1268.90			4.57				
74+00	1269.20			4.27				
+50	1269.50		C-0.5	3.97	1270.00	T.P.	BM#7 1274.57	1274.55
75+00	1269.80	6.86	1276.80	7.02				
+50	1270.22		1276.82	6.60				
76+00	1270.88			5.94				
+50	1271.78			5.04				
77+00	1272.92			3.90	1272.92	T.P.		
+50	1274.30	10.83	1283.75	9.45				
78+00	1275.93			7.82				
+50	1277.79			5.76				
79+00	1279.89			3.86				

1266.55
1.72
1264.83
8.64
1273.47
3.47
1270.00
6.86
1276.80
2.25
1274.55

1274.57
2.25
1276.82
3.90
1272.92
10.83
1283.75

Stg		BS	HI	FS		
			1283.75			
79+50	1282.11			1.64	FOS	
80+00	128408	8.85	1290.45	6.37	FOS	
+50	1285 53			4.92		
81+00	1286.46			3.99		
+50	1286.90			3.55	1286.89	T.P.
82+00	125680					

1283.75
2.15
1281.60 TP 1281.60
8.85
1290.45
3.56
1286.89

Finished Grade TP Sta 81+50 1286.89

Sta		B.S.	H.I	F.S.	Elev	
82+00	1286.80	3.53	1290.42	3.62		
+50	1286.20			4.22		
83+00	1285.08			5.34		
+50	1283.45			6.97		
84+00	1281.56			8.86		
+50	1279.68			10.74	1279.68	T.P
85+00	1277.80	1.20	1280.88	3.08		
+50	1275.92			4.96		
86+00	1274.04			6.84		
+50	1272.16			8.72		
87+00	1270.28			10.60	1270.28	T.P
+50	1268.40	0.57	1270.85	2.45		
88+00	1266.52			4.33		
+50	1264.64			6.21		
89+00	1262.76			8.09		
+50	1260.88			9.97		
90+00	1259.00			11.85	1259.00	T.P
		1.85	1260.85			B.M. #.05
				4.16	1256.69	1256.74

Winnin Spohn 10/30/28

1286.89
3.53
1290.42
10.74
1279.68
1.20
1280.88
10.60
1270.28
0.57
1270.85
1.85
1259.00
1.85
1260.85
4.16
1256.69

		1257.10				
93			9.38	1247.72	F 1.8 / 21.2	C 0.0 / 23.7
94			12.48	1244.62	F 0.6 / 23.7	C 1.9 / 26.8
	2.54	1246.56	13.08	1244.02		
95			4.41	1242.15	C 0.7 / 26.2	C 3.2 / 29.9
96			6.36	1240.20	F 0.1 / 24.6	C 2.3 / 27.9
97			7.97	1238.59	F 0.8 / 22.8	C 0.8 / 25.0
	0.26	1238.51	8.31	1238.25		
98			0.99	1237.52	F 1.2 / 22.1	F 0.6 / 23.1
99			2.05	1236.46	F 1.7 / 21.3	F 0.8 / 22.5
100			3.11	1235.40	F 2.4 / 21.5	F 1.3 / 21.6
101			3.95	1234.56	F 3.2 / 22.5	F 2.0 / 20.5
102			4.81	1233.70	F 2.8 / 23.1	F 1.8 / 20.6

		1238.51			
103			5.66	1232.85	
	2.62	1235.78	5.36	1233.16	
104			4.32	1231.46	
BM #9	2.33	1235.75	2.33	1233.45	1232.42
105			7.05	1228.70	
106			11.57	1224.18	
	0.98	1224.56	12.17	1223.58	
107			6.37	1218.19	
	6.33	1218.22	12.67	1211.89	
108			6.76	1211.46	
	2.64	1208.30	12.56	1205.66	
109			3.30	1205.00	
110			7.91	1200.91	
	6.85	1202.15	13.00	1195.30	
111			4.18	1197.97	
112			4.75	1197.40	

C 0.3 / 23.6

C 1.5 / 25.2

C 1.4 / 25.6

C 0.4 / 24.3

C 3.1 / 28.3

C 1.2 / 25.9

C 7.4 / 34.0

F 0.5 / 24.3

C 5.8 / 32.1

C 0.2 / 24.6

C 4.6 / 32.4

F 3.9 / 22.7

F 2.9 / 23.7

F 5.7 / 27.3

F 5.1 / 23.9

F 3.2 / 24.6

F 3.8 / 22.5

F 1.3 / 22.4

F 2.2 / 20.7

C 2.6 / 28.2

		1202.15			
113			5.05	1197.10	
114			5.35	1196.80	
	5.90	1199.50	8.55	1193.60	
115			3.00	1196.50	
116			3.20	1196.20	
117			3.60	1195.90	
118			3.90	1195.60	
	2.25	1199.24	2.51	1196.99	
119			3.94	1195.30	
120			4.72	1194.52	
BM#10	0.24	1196.79	2.73	1196.51	1196.55
121			3.99	1192.80	
122			5.99	1190.80	

C 0.3 / 24.6

C 2.3 / 27.7

F 3.2 / 21.7

F 1.3 / 22.9

F 2.8 / 20.7

F 0.5 / 23.6

F 2.4 / 20.5

F 0.6 / 22.8

F 2.9 / 20.5

F 1.0 / 22.5

C 1.4 / 26.2

C 2.2 / 26.8

C 0.7 / 25.3

C 1.5 / 26.2

C 1.4 / 26.4

C 0.9 / 25.0

C 0.5 / 24.6

C 0.1 / 24.7

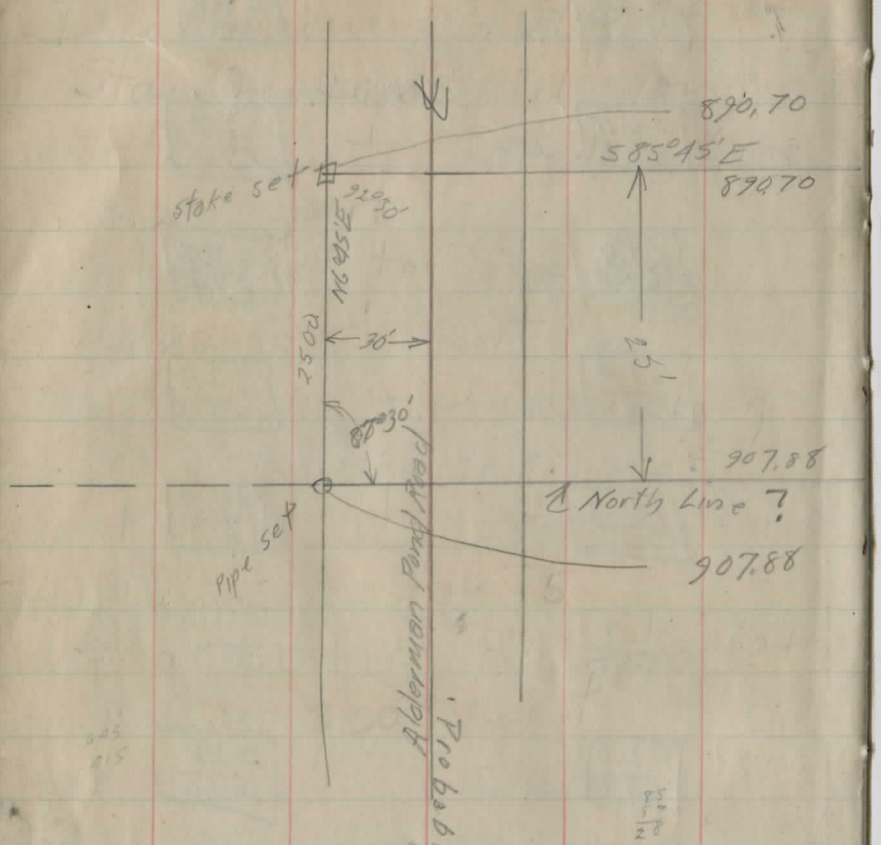
F 0.3 / 24.0

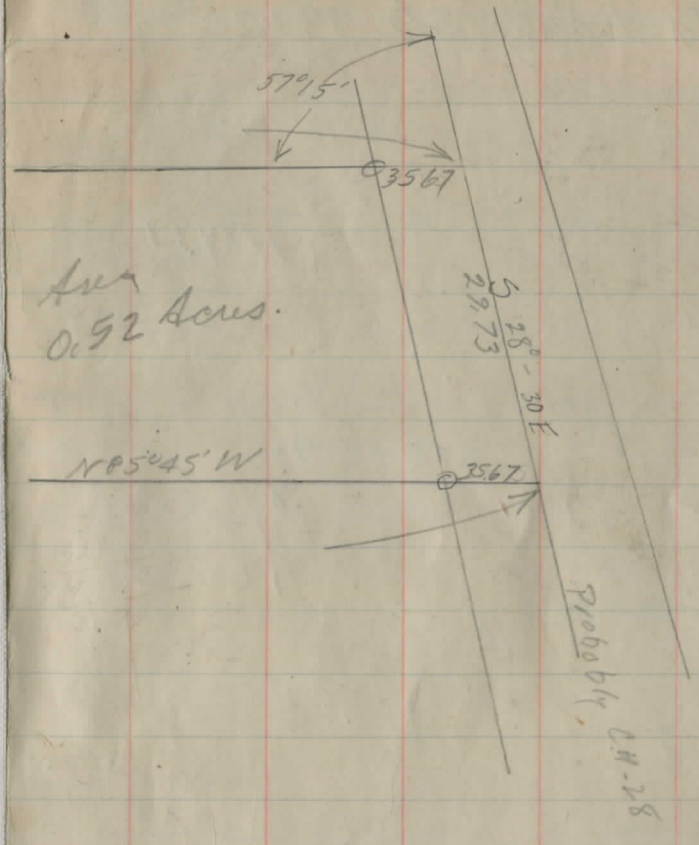
F 0.5 / 23.6

		1196.79				
123			7.99	1188.80	F 0.8 / 23.6	C 0.2 / 25.0
	2.65	1190.66	8.78	1188.01		
124			3.96	1186.70	F 0.5 / 24.3	C 2.0 / 27.4
125			6.64	1184.02	C 1.8 / 26.5	C 3.4 / 29.4
126			9.89	1180.77	C 1.6 / 26.2	C 3.8 / 29.7
	0.57	1180.04	11.19	1179.47		
127			2.55	1177.49	F 1.2 / 22.0	F 1.9 / 21.5
128				1175.96	34.8	31.3
129			5.33	1179.71	F 2.0 / 21.8	C 0.0 / 24.0
Tem	10.20	1184.91	5.33	1179.71		
130				1175.10	30.3	31.2
			2.34	1182.57	1182.71	

10.20

Survey of Right-of-Way for Claridon Twp Trustees on Buchner Property





85-45
6 AC
92 30
87-30

6/9/28 Richey Whisman Parks Spohn

Restaked bridge Sta. 33+26

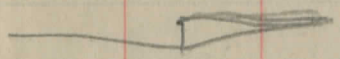


Table IX.—Calculation of Earthwork.

Width	Height														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	.02	.04	.06	.07	.09	.11	.13	.15	.17	.18	.20	.22	.24	.26	.28
2	.04	.07	.11	.15	.18	.22	.26	.30	.33	.37	.41	.44	.48	.52	.56
3	.06	.11	.17	.22	.28	.33	.39	.44	.50	.56	.61	.67	.72	.78	.83
4	.07	.15	.22	.30	.37	.44	.52	.59	.67	.74	.81	.89	.96	1.04	1.11
5	.09	.19	.28	.37	.46	.56	.65	.74	.83	.93	1.02	1.11	1.20	1.30	1.39
6	.11	.22	.33	.44	.56	.67	.78	.89	1.00	1.11	1.22	1.33	1.44	1.55	1.67
7	.13	.26	.39	.52	.65	.78	.91	1.04	1.16	1.30	1.42	1.55	1.68	1.81	1.94
8	.15	.30	.44	.59	.74	.89	1.04	1.19	1.33	1.48	1.63	1.78	1.92	2.08	2.22
9	.17	.33	.50	.67	.83	1.00	1.17	1.33	1.50	1.67	1.83	2.00	2.17	2.33	2.50
10	.18	.37	.56	.74	.93	1.11	1.30	1.48	1.67	1.85	2.04	2.22	2.41	2.59	2.78
11	.20	.41	.61	.82	1.02	1.22	1.43	1.63	1.83	2.04	2.24	2.44	2.65	2.85	3.06
12	.22	.44	.67	.89	1.11	1.33	1.56	1.78	2.00	2.22	2.44	2.67	2.89	3.11	3.33
13	.24	.48	.72	.96	1.20	1.44	1.68	1.92	2.16	2.41	2.65	2.89	3.13	3.37	3.61
14	.26	.52	.78	1.04	1.30	1.55	1.81	2.08	2.33	2.59	2.85	3.11	3.37	3.63	3.89
15	.28	.56	.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	3.06	3.33	3.61	3.89	4.17
16	.30	.59	.89	1.18	1.48	1.78	2.07	2.37	2.67	2.96	3.26	3.56	3.85	4.15	4.44
17	.31	.63	.94	1.26	1.57	1.89	2.20	2.52	2.83	3.15	3.46	3.78	4.09	4.41	4.72
18	.33	.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	3.67	4.00	4.33	4.67	5.00
19	.35	.70	1.06	1.41	1.76	2.11	2.46	2.82	3.17	3.52	3.87	4.22	4.57	4.92	5.28
20	.37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	4.07	4.44	4.81	5.18	5.56
21	.39	.78	1.17	1.55	1.94	2.33	2.72	3.11	3.50	3.89	4.28	4.67	5.06	5.44	5.83
22	.41	.81	1.22	1.63	2.04	2.44	2.85	3.26	3.67	4.07	4.48	4.89	5.30	5.70	6.11
23	.43	.85	1.28	1.70	2.13	2.56	2.98	3.41	3.83	4.26	4.68	5.11	5.54	5.96	6.39
24	.44	.89	1.33	1.78	2.22	2.67	3.11	3.56	4.00	4.44	4.89	5.33	5.78	6.22	6.67
25	.46	.92	1.39	1.85	2.31	2.78	3.24	3.70	4.17	4.63	5.09	5.56	6.02	6.48	6.94
26	.48	.96	1.44	1.92	2.41	2.89	3.37	3.85	4.33	4.82	5.30	5.78	6.26	6.74	7.24
27	.50	1.00	1.50	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00	6.50	7.00	7.50
28	.52	1.04	1.55	2.07	2.59	3.11	3.63	4.15	4.67	5.18	5.70	6.22	6.74	7.26	7.78
29	.54	1.07	1.61	2.15	2.68	3.22	3.76	4.30	4.83	5.37	5.91	6.44	6.98	7.52	8.06
30	.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.55	6.11	6.67	7.22	7.78	8.33
31	.57	1.15	1.72	2.30	2.87	3.44	4.02	4.59	5.17	5.74	6.32	6.89	7.46	8.04	8.61
32	.59	1.18	1.78	2.37	2.96	3.56	4.15	4.74	5.33	5.92	6.52	7.11	7.70	8.30	8.89
33	.61	1.22	1.83	2.44	3.05	3.67	4.28	4.89	5.50	6.11	6.72	7.33	7.94	8.55	9.17
34	.63	1.26	1.89	2.52	3.15	3.78	4.40	5.04	5.67	6.29	6.93	7.56	8.18	8.81	9.44
35	.65	1.30	1.94	2.59	3.24	3.89	4.53	5.18	5.83	6.48	7.13	7.78	8.42	9.08	9.72
36	.67	1.33	2.00	2.67	3.33	4.00	4.66	5.33	6.00	6.67	7.33	8.00	8.67	9.33	10.00
37	.68	1.37	2.06	2.74	3.42	4.11	4.79	5.48	6.17	6.85	7.54	8.22	8.91	9.59	10.28
38	.70	1.41	2.11	2.82	3.52	4.22	4.92	5.63	6.33	7.03	7.74	8.44	9.15	9.85	10.56
39	.72	1.44	2.17	2.89	3.61	4.33	5.05	5.78	6.50	7.22	7.95	8.67	9.39	10.11	10.83
40	.74	1.48	2.22	2.96	3.70	4.44	5.18	5.92	6.67	7.41	8.15	8.89	9.63	10.37	11.11

Table gives cu. yds. in 1 ft. of a triangle of given width and height. Corrections for tenths of width are one tenth the values found under each height considering the widths from 1 to 9 as tenths and similarly the corrections for tenths of height are one tenth the figures opposite width considering the heights from 1 to 9 as tenths. Thus if w =16.2 and h =5.3, cu. yds. =1.48+.028+.089 =1.597 cu. yds. or practically 160 cu. yds. per 100 ft. If w exceeds 40 ft., use one half and multiply result by 2, if both w and h are large use one half of each and multiply result by 4. Any cross-section may be divided into triangles by the following rule. To the triangle of the sum of the outside cuts (or fills) =h, and ½ the roadbed =w, add the triangles formed by taking the distance out to each break in turn (=w's) by the difference between the cuts (or fills) on each side of it (=h's), always subtracting the outer from the inner.

Distances from Center of Roadway for Cross-Sectioning.

Roadway 16 feet wide. Side Slopes 1 on 1½.

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	25.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20—16)÷2 or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.

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